

# Predictive quantification of surrogate model fidelity based on modal variations with sample density

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**Abstract** It is generally challenging to quantify the fidelity of surrogate models without additional system evaluations. Standard error measures, such as the mean squared error and cross-validation error, often do not adequately capture the fidelity of the model trained using all available sample points. This paper introduces a new model-independent approach to quantify surrogate model fidelity, called Predictive Estimation of Model Fidelity (PEMF). In PEMF, intermediate surrogates are iteratively constructed over heuristic subsets of sample points. The median and the maximum errors estimated over the remaining points are used to determine the respective error distributions at each iteration. The estimated modes of the error distributions are represented as functions of the density of intermediate training points through nonlinear regression, assuming a smooth decreasing trend of errors with increasing sample density. These regression functions are then used to predict the expected median and maximum errors in the final surrogate model (trained using all available sample points). A Monotonic Trend criterion is defined to statistically test if

the regression function is reasonably reliable in predicting the model fidelity, failing which a stable implementation of k-fold cross-validation (based on modal error) is used to predict the final surrogate error. To compare the accuracy and robustness of PEMF with that of the popular leave-one-out cross-validation, numerical experiments are performed using Kriging, RBF, and E-RBF models. It is observed that the model fidelities estimated by PEMF is up to two orders of magnitude more accurate and statistically more stable compared to those based on cross-validation.

**Keywords** Surrogate model · Model fidelity · Error estimation · Uncertainty quantification · Kriging · Radial basis functions

## 1 Introduction

### 1.1 Approximation models

Mathematical approximation models are commonly used to provide a tractable and inexpensive approximation of the actual system behavior in many routine engineering analysis and design activities, e.g., domain exploration, sensitivity analysis, development of empirical models, and optimization. One of the most popular classes of approximation models are surrogate models or metamodels (Kleijnen 1975), which are purely mathematical models, and are not directly derived from the physics of the system being modeled. Major surrogate modeling methods include Polynomial Response Surfaces (Jin et al. 2000), Kriging (Simpson et al. 2001; Forrester and Keane 2009), Radial Basis Functions (RBF) (Hardy 1971), Neural Networks (Yegnanarayana 2004), Support Vector Regression (Gunn 1998), and hybrid surrogate models (Queipo et al.

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2005; Zhang et al. 2012). Constructing a surrogate model typically involves the following steps:

1. Performing a design of experiments (DOE);
2. Executing the sample experiments (e.g., high fidelity simulations or physical experiments) to generate the training data;
3. Selecting and training the appropriate surrogate model using the training data; and
4. Testing the accuracy of the surrogate model.

In the fourth step, specialized error measures can be used to assess the accuracy of the surrogate model in representing the actual system behavior. The knowledge of the regional and global accuracy of a surrogate is crucial (i) for model selection, (ii) for further improvement of the surrogate, e.g., using adaptive sampling (Lehmensiek et al. 2002) or active learning (Sugiyama 2006), (iii) for iterative surrogate-based optimization (Jones et al. 1998; Mehmani et al. 2012), and (iv) for quantifying the uncertainty associated with the surrogate. Other possible applications include the construction of hybrid surrogate models and conservative surrogate models. The state-of-the-art measures of surrogate model error are subject to one or more of the following limitations:

- They are model-dependent (and hence may not be suitable for global model comparison, and effective model selection); or
- They require additional system evaluations (and hence are expensive); or
- They quantify errors in intermediate surrogates (e.g., PRESS), which are often not representative of the error in the actual surrogate model that will be used for design and analysis; and
- They generally do not provide an understanding of the uncertainty introduced by a surrogate model in a design process (i.e., instead provides deterministic error measures).

In this paper, we conceive and develop a new error quantification method for surrogate models that seek to address the above limitations. In the following subsection, the existing major methods for assessing the accuracy of surrogates are briefly reviewed.

## 1.2 Measures of surrogate model fidelity

Methods for quantifying the fidelity of or (inversely) the error in statistical models can be broadly classified into: (i) methods that require additional data, and (ii) methods that use existing data (Meckesheimer et al. 2002). The former can be significantly expensive and is thus not a practical option in a majority of surrogate modeling applications. Error quantification methods can also be classified into global and local error estimation methods (Goel et al. 2007). The performance of the surrogate over the entire

domain is evaluated by global error measures, while local or point-wise error measures provide the surrogate accuracy in different locations of the design domain. Table 1 provides a list of popular surrogate modeling methods, and the error estimation techniques commonly used for these surrogates.

Popular approaches to quantifying model independent global error measures include (Queipo et al. 2005): split sample, cross-validation, bootstrapping, and Akaike's information criterion (AIC) method. In a split sample strategy, the sample data is divided into training and test data. The former is used to construct a surrogate; and the latter is used to test the performance of the surrogate. Cross-validation is a popular technique to estimate the error of a surrogate without investing any additional system evaluations. In  $q$ -fold cross-validation approach, the data set is split randomly into  $q$  (approximately) equal subsets. The surrogate is constructed  $q$  times, each time leaving out one of the subsets from the training set. The omitted subset, at each iteration, is used to evaluate the cross-validation error (Viana et al. 2009). A  $k$ -fold cross-validation approach is a variation of  $q$ -fold approach, in which all the possible subsets of size  $k$  are used to evaluate cross-validation error. In *leave-one-out cross-validation* approach ( $k = 1$ ), at each iteration the training set is created by using all sample points except one, and the left out point is used for estimating the error between the surrogate prediction and the actual value. The bootstrapping approach generates  $m$  sub-samples from the sample points. Each sub-sample is a combination of all samples with replacement. Different variants of the bootstrapping approach can be used for model identification and determining confidence intervals for surrogates (Queipo et al. 2005). In Akaike's original AIC, the performance of the surrogate was predicted based on a penalized likelihood. AIC is equal to the sum of a negative log likelihood and a penalty term, as given by

$$AIC = -2 \log L(\hat{\theta}) + 2k \quad (1)$$

In this equation,  $L(\hat{\theta})$  is the maximized likelihood function, and  $k$  is the number of free parameters in the model, which is a measure of complexity or the compensation for the bias in the lack of fit when the maximum likelihood estimators are used (Bozdogan 2000).

Standard local error measures include: (i) the mean squared errors for Kriging (Jones et al. 1998), and (ii) the linear reference model (LRM) (Nguyen et al. 2011). In stochastic surrogate models like Kriging, the errors at two different points of the design domain are not independent; and the correlation between the points is related to the distance between them. When the distance between the two points is smaller, the correlation tends to one, and when the distance is larger, the correlation tends to zero. According to this correlation strategy, if the point  $x^*$  is close to sample points, the prediction confidence at that point is higher

**Table 1** Techniques for surrogate model construction and validation

	RMSE	F-test	ANOVA	Split sample	Bootstrapping	Cross-validation	AIC
PRS	✓	✓	✓				✓
Kriging	✓	✓	✓	✓	✓	✓	
RBF				✓	✓	✓	
E-RBF				✓	✓	✓	
ANN	✓	✓	✓				
SVR	✓	✓	✓				✓

than that when the point is far away from all the sample points. This concept is reflected in the local error measurement method for Kriging predictor at the special point  $x^*$ . This error is equal to zero at the sample points and is equal to the approximation error variance in the stochastic process. The LRM is a model independent method for quantifying the local performance of a surrogate. The LRM considers the region with oscillations as a high-error location. This method categorizes errors of a surrogate in the design domain based on the deviation of the surrogate from the local linear interpolation (Nguyen et al. 2011).

Another popular cross-disciplinary error measure is the mean squared error (MSE) or root mean square error (RMSE), which provides a measure of global error over the entire design domain. The RMSE evaluated at a set of test points ( $N_{Test}$ ) is given by:

$$RMSE = \sqrt{\frac{1}{N_{Test}} \sum_{i=1}^{N_{Test}} (y_i - \hat{y}_i)^2} \tag{2}$$

where  $y_i$  and  $\hat{y}_i$  are the actual and the predicted values at the  $i^{th}$  test point, respectively. The RMSE thus provides information about the accuracy of the actual surrogate. However RMSE requires additional system evaluations at test points in the case of interpolating surrogates. The maximum absolute error (MAE) and relative absolute error (RAE) are indicative of local deviations:

$$MAE = \max_{i=1, \dots, N_{Test}} |y_i - \hat{y}_i| \tag{3}$$

$$RAE_i = \left| \frac{y_i - \hat{y}_i}{y_i} \right| \tag{4}$$

The prediction sum of square (PRESS) is based on the *leave-one-out cross-validation* error:

$$PRESS = \frac{1}{N} \sum_{i=1}^N (\hat{y}_i - \hat{y}_i^{(-i)})^2 \tag{5}$$

where  $\hat{y}_i$  and  $\hat{y}_i^{(-i)}$  are the surrogate estimations at the  $i^{th}$  training point respectively predicted by the surrogate constructed using all sample points and the surrogate constructed using all sample points except the  $i^{th}$  point (Queipo et al. 2005). Goel et al. (2009) and Goel and Stander (2009) compared different error measures including

PRESS and MSE for Kriging, and found that PRESS provided better performance compared to the other methods, as a fidelity prediction and as a surrogate model selection criterion.

Meckesheimer et al. (2002) used the root mean square error of  $k$ -fold cross-validation ( $RMSE_{CV}$ ), i.e., root mean square of PRESS ( $PRESS_{RMS}$ ), to measure the global accuracy of the surrogate over the entire design domain:

$$RMSE_{CV} = \sqrt{\frac{1}{k} \sum_{i=1}^k (\hat{y}_i - \hat{y}_i^{(-i)})^2} \tag{6}$$

where  $k$  is the number of omitted sample points. The variation of  $k$  from 1 to 10 was studied; for each  $k$  value, the average of the error measured on all possible combinations of  $k$  points were used to provide a measure of the global accuracy of the surrogate. They also compared this error measure with the actual error estimated on additional test points to show the practicality of the  $RMSE_{CV}$  as a fidelity characterizing method without using additional system evaluations.

Viana et al. (2009) applied the  $RMSE_{CV}$  approach as a criterion in surrogate model selection and in constructing a weighted average surrogate. They also showed that better results can be achieved using the *leave-one-out* approach. Later, Viana et al. (2010) used  $RMSE_{CV}$  to estimate the safety margin for a conservative surrogate model. Zhang et al. (2014) applied relative absolute error of cross-validation ( $RAE_{CV}$ ) for characterizing the uncertainty in surrogate models, where the normalized  $RAE_{CV}$  at the  $i^{th}$  training point is defined based on the *leave-one-out* approach. This characterization was used in conjunction with support vector machines to segregate the design space into sub-spaces based on the level of model errors.

### 1.3 Model refinement using surrogate error measures

Another important area of application of surrogate model error measures is “model refinement”. Over the last two decades, different statistical strategies have been developed to improve the accuracy and robustness of surrogate models by adding infill points where additional evaluations of the high fidelity model / experiment are desired to be

performed. Infill points can be added in a fully sequential manner (one-at-a-time), or can be added in a batch sequential manner.

In the literature, there exist various criteria for determining the locations of the infill points (Jones et al. 1998; Williams et al. 2011; Keane 2006; Booker et al. 1999; Audet et al. 2000). Jin et al. (2002) reviewed different one-at-a-time sequential sampling criteria, and illustrated their potential benefits over single stage methods (McKay et al. 1979; Sacks et al. 1989). Among the sequential sampling methods that are not limited to a specific surrogate model types, Kleijnen and Beers (2004) used *cross-validation* error and Jackknifing variance as infill points criteria (Meckesheimer et al. 2002). This method evaluates the variance between the estimations of the surrogate model and the high fidelity model /experiment and subsequently adds points in the area with the highest variance. Loepky et al. (2010) explored different batch and one-at-a-time sequential criteria for the Gaussian process model. They pointed out that these criteria perform better under the batch sequential approach, and one-at-a-time augmentation would be likely impractical due to the higher computational cost (especially in the case of physical experiments).

Williams et al. (2011) applied different batch sequential criteria to achieve *stability* in the fidelity of a Gaussian process (GP) model that is used in the ‘Bayesian Calibration of Computer Models’ (Kennedy and O’Hagan 2000). This GP model is trained using the disagreement between the output values given by experiments and the computer model on infill points; in this case *stability* implies the phase where adding more infill points has a minimal influence on the accuracy of the GP model (Atamturktur et al. 2011). Atamturktur et al. (2013) assessed the ability to improve the fidelity of the computer model using different index-based and distance-based batch sequential sampling criteria through a powerful quantitative Predictive Maturity Index (PMI) metric, developed earlier by Hemez et al. (2010). The proposed PMI could guide decision makers to allocate resources (infill points), and track the progress in the improvement of a predictive capability (Atamturktur et al. 2011; Atamturktur et al. 2013).

It can be readily concluded from the research reported in the existing literature that, there is a need for reliable and statistically stable measures of surrogate model fidelity, to facilitate improvement or informed application of surrogates in design and analysis. More specifically, it is necessary for such error quantification approaches to have the following characteristics:

- (i) Be independent of the type of model (e.g., Radial basis function, Polynomial response surface, Gaussian processes), so as to allow fair and competitive model selection;
- (ii) Provide a predictive estimate of the error of the actual model, instead of the (mean or RMS) error of intermediate surrogates; and
- (iii) Provide a measure of error that is minimally sensitive to outlier sample points.

The method presented in this paper seeks to directly incorporate these much-needed characteristics into quantification of error in surrogate models. The objectives of developing a new surrogate model error quantification method are summarized in the next subsection.

#### 1.4 A new predictive and model-independent approach to model error quantification

The method developed in this paper, called Predictive Estimation of Model Fidelity (PEMF), is designed to address two primary objectives. The first objective is to develop a model-independent methodology for quantifying the fidelity of the ‘*actual surrogate*’ without requiring additional system evaluations. In this context, the ‘actual surrogate’ refers to the surrogate model constructed using all available training points (and not any subset of training points, as used in cross-validation). With this approach, we provide error information for the actual model that is to be used for function analysis or optimization (assuming surrogate model construction is not an end in itself). The second objective is to track the variation of the surrogate model error with an increasing density of training points, thereby creating opportunities for global model selection and model refinement. The investigation of these latter opportunities are however not within the scope of this paper.

The paper is organized as follows: the formulation of the proposed model fidelity quantification approach is described in Section 2; numerical experiments and results are respectively presented in Sections 3 and 4. In Section 5, statistical tests are performed on the PEMF method. Concluding remarks and future work are provided in Section 6.

## 2 Predictive estimation of model fidelity (PEMF)

### 2.1 Predictive estimation of model fidelity

The PEMF method determines the model fidelity within the design domain (defined by the user) by analyzing the variation in the model error distribution with increasing number of training points. This measure of fidelity can provide uniquely useful information about the accuracy of the surrogate in regions of interest or the entire design domain, thereby significantly improving the usability of

the surrogates in model-based design applications. In the context of surrogate-based design, this information can be directly applied for (i) surrogate model refinement (Atamturktur et al. 2013; Jin et al. 2002; Kleijnen and Beers 2004), (ii) surrogate model selection (Chowdhury et al. 2014a; Gorissen et al. 2009; Martin and Simpson 2005), and (iii) uncertainty analysis (Chowdhury et al. 2014b; Allaire et al. 2012). In these applications, PEMF is either enabling more informed use of the constructed surrogate model or the platform to identify and use the surrogate model that is most suited to the concerned design process. A flowchart describing the PEMF algorithm is illustrated in Fig. 1, and the major steps are described below:

2.1.1 Generating sample data

In this step, a set of experimental designs are generated based on a user-specified distribution or given by a DOE. The expensive system evaluation (simulation or physical experiments) is then performed over the sample data points. The entire set of sample points is represented by  $\{X\}$ . This sample input-output data might also be given by other measured data sources.

2.1.2 Defining the region of interest

The entire set of sample points is divided into inside and outside sets based on the boundaries of the user-defined region of interest, and are represented by  $\{X_{in}\}$  and  $\{X_{out}\}$ , respectively.

2.1.3 Quantifying the variation of the error distribution with sample density

This step is an iterative process, where the number of iterations ( $N^{itr}$ ) is to be guided by the dimension of the problem, the number of sample points in the inside set, and the observed stability of error variation. In this first development and implementation of PEMF (in this paper) the number of iterations will be fixed (prescribed by the user). At each iteration, sample points are divided into a set of intermediate training data  $\{X_{TR}\}$  and a set of intermediate test data  $\{X_{TE}\}$ , i.e.,

$$\begin{aligned} \{X_{TR}^t\} &= \{X_{out}\} + \{\beta^k\} \\ \{X_{TE}^t\} &= \{X\} - \{X_{TR}^t\} \\ \text{where, } \{\beta_i^t\} &\subset \{X_{in}\} \\ t &= 1, 2, 3, \dots, N^{itr} \end{aligned} \tag{7}$$

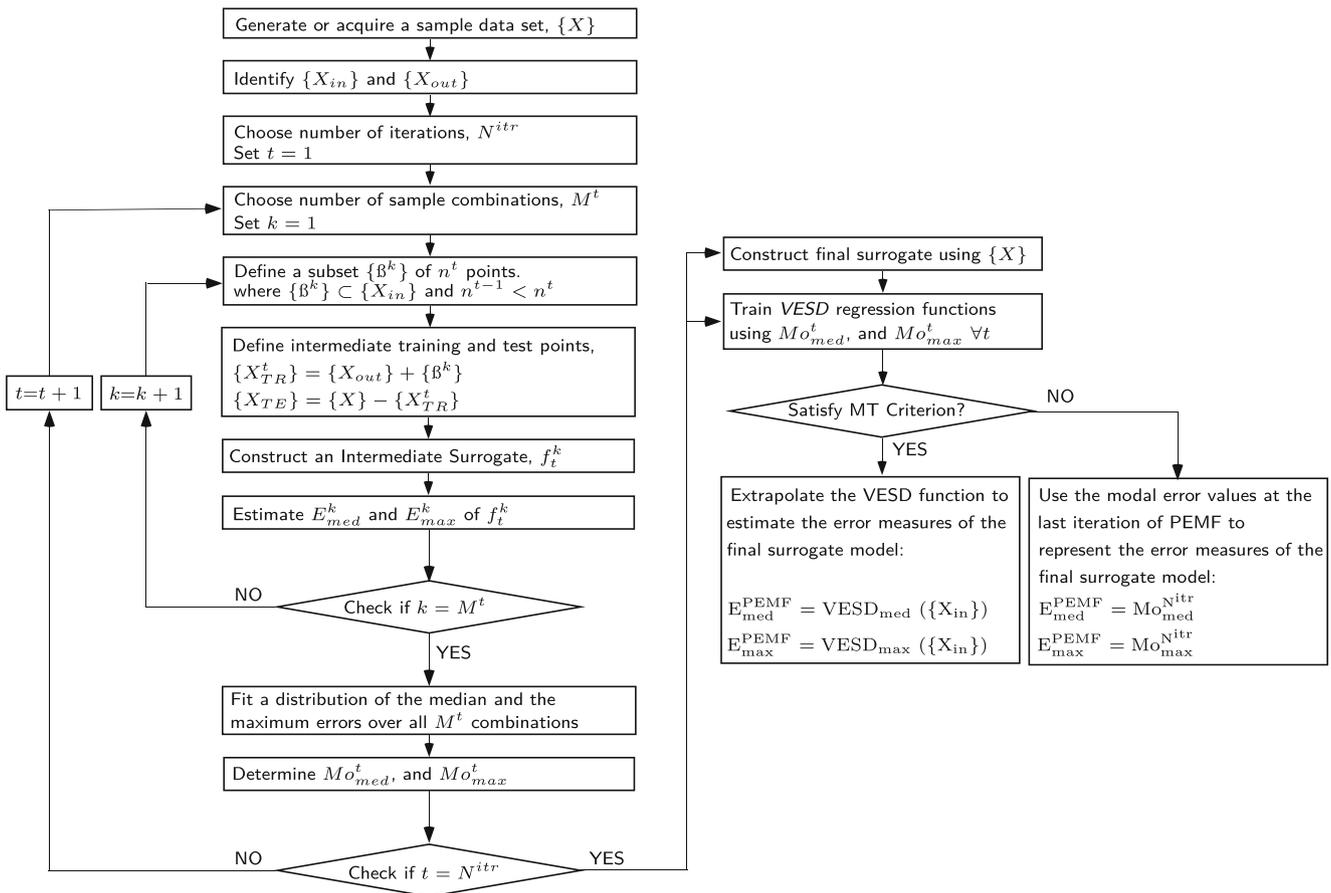


Fig. 1 The Predictive Estimation of Model Fidelity (PEMF) algorithm

where  $\{B^k\}$  represents a  $k^{th}$  subset of inside-region sample points. At each iteration  $t$ , the size of  $\{B^k\}$  is defined by  $n^t$ , where  $n^{t+1} > n^t$  and  $n^1 \geq 1$ .

At each iteration, the total number of possible sample combinations is defined by  $M^t$  where  $M^t \leq \binom{N_i}{n^t}$ ; the term  $N_i$  represents the number of inside-region sample points. In low dimensional problems, all possible subsets of size  $n^t$  could be used, while in high dimensional problems, a fraction of subsets could be used to avoid intractable computational cost. Intermediate surrogates  $f_t^k$ , are constructed at the  $t^{th}$  iteration for all combinations,  $k = 1, 2, \dots, M^t$ , using the intermediate training points. These surrogates are then evaluated over the intermediate test points.

The median and the maximum errors for each combination ( $E_{med}^k$  and  $E_{max}^k$ ) are then estimated using the RAE values on the intermediate test points ( $e_1, e_2, \dots, e_{m^t}$ ). Probability distribution functions are used to represent the distribution of the median and the maximum errors over the  $M^t$  different combinations at each iteration, thereby providing an understanding of the uncertainty directly associated with the surrogate model. A chi-square ( $\chi^2$ ) goodness-of-fit criterion (Haldar and Mahadevan 2000) is used to select the most suitable type of distribution from a list of candidates such as lognormal, Gamma, Weibull, logistic, log logistic,  $t$  location scale, inverse Gaussian, and generalized extreme value distribution. The  $\chi^2$  criterion is defined based on the error between the observed and the assumed PDF of the distribution. Assuming the observed frequencies of  $m$  intervals of the random variable are represented by  $o_1, o_2, \dots, o_m$ , the corresponding theoretical frequencies are represented by  $t_1, t_2, \dots, t_m$ ; and the  $\chi^2$  criterion is given by

$$\chi^2 = \sum_{i=1}^m \frac{(o_i - t_i)^2}{t_i} \quad (8)$$

The mode of the median and the maximum error distributions at each iteration ( $Mo_{med}^t$  and  $Mo_{max}^t$ ) are evaluated to provide a measure of central tendency, and are used to relate the variation of the surrogate error with the sample density.

#### 2.1.4 Predicting the fidelity of the final surrogate

The final surrogate model is constructed using the entire set of training data. Regression models are applied to represent the statistical mode of the median error distribution ( $Mo_{med}$ ) and that of the maximum error distribution ( $Mo_{max}$ ) at each iteration as monotonic functions of the number of inside-region training points,  $n^t$ . These regression functions are called the *variation of error with sample density* (VESD), and are expressed as

$$\begin{aligned} {}^t E_{med}^{Mo} &= F_{med}(n^t) \\ {}^t E_{max}^{Mo} &= F_{max}(n^t) \end{aligned} \quad (9)$$

The VESD regression functions are then used to predict the fidelity of the final surrogate model under the condition that a Monotonic Trend (MT) Criterion is satisfied. The MT criterion is defined to statistically test the feasibility of a monotonic decrease of the model fidelity with increasing sample density. If the MT criterion is not satisfied, a stable implementation of the  $k$ -fold cross-validation (PEMF-based  $k$ -fold) is used instead of the VESD functions to represent the surrogate model fidelity. The formulation and application of the MT criterion is described in the following subsection.

### 2.2 Constructing and testing functions to represent the variation of error with sample density (VESD)

The selection of the type of regression function is critical to quantify the variation of error with training point density. In this paper, two types of regression functions are used to represent the variation of maximum and median errors as functions of the number of inside-region training points. These functions are

Type 1 Exponential regression function

$$F(n^t) = a_0 e^{-a_1 (n^t)} \quad (10)$$

Type 2 Multiplicative regression function

$$F(n^t) = a_0 (n^t)^{-a_1} \quad (11)$$

where  $a_0$  and  $a_1$  are regression coefficients known as initial value and rate of decay, respectively. These coefficients are determined using the least square method such that  $a_0, a_1 > 0$ , and  $n^t \geq 1$ . The smaller the rate of decay ( $a_1$ ), the lower the sensitivity of surrogate accuracy to sample density. Numerical experiments exploring linear, polynomial, multiplicative, exponential, and other standard regression functions indicated that exponential and multiplicative functions are the most suitable choice in this context. In this paper, the root mean squared error metric is used to select the best-fit regression model. The choice of these regression functions assume a smooth monotonic decrease of the model error with increasing density or number of training points within the region of interest.

Intuitively, most surrogate modeling scenarios are expected to conform to the monotonically decreasing trend of the model error (with sample density). However, in certain cases, the variation of the estimated error ( $Mo_{med}^t$  and  $Mo_{max}^t$ ;  $t = 1, 2, \dots, N^{itr}$ ) with sample density (over iterations) may not follow the monotonically decreasing trend. Such cases may arise due to a highly non-uniform distribution of sample points or a highly skewed distribution of nonlinearity of the actual output function over the input space. To consider the possibility of such non-conforming

cases, and to avoid unreasonable inaccuracies in error predictions using the fitted VESD function, the feasibility of the monodically decreasing trend of model error is statistically tested using a criterion called the *Monotonic Trend* (MT) criterion. If the MT criterion is satisfied by the fitted VESD regression function, this VESD function is considered admissible and is used to predict the error in the final surrogate (constructed over all sample points). Otherwise, a stable implementation of  $k$ -fold cross-validation, called *PEMF-based  $k$ -fold cross-validation*, is used to represent the error in the final surrogate model. The *PEMF-based  $k$ -fold cross-validation* method is defined as the modal value of the error of the intermediate surrogate constructed using  $n^{N^{itr}}$  sample points (i.e., the modal error value in the last iteration of PEMF). The median and the maximum error measures of the final surrogate are then respectively given by  $Mo_{med}^{N^{itr}}$  and  $Mo_{max}^{N^{itr}}$  (as is further defined in (16)).

In the MT test, we use the Pearson correlation coefficient (Lawrence and Lin 1998) to measure the linear correlation between the log-level and the log-log transformation of *Error* with respect to the *Sample density* in the Type 1 and Type 2 VESD functions. In this test, the following standard mathematical properties are employed:

- (i) if a  $(x, y)$  input/output data set follows an exponential relationship, the transformed  $(x, \log y)$  data follows a linear relationship, and
- (ii) if a  $(x, y)$  input/output data set follows a purely  $p^{th}$  order power relationship, the transformed  $(\log x, \log y)$  data follows a linear relationship.

In this test, the Pearson coefficient for the Type 1 and Type 2 VESD functions is defined as:

$$\rho_{\lambda,\varphi} = \frac{Cov(\lambda,\varphi)}{\sigma_\lambda \sigma_\varphi} \tag{12}$$

where

$$\lambda = \ln(Mo^{t=1,2,\dots,N^{itr}}) \tag{13}$$

$$\varphi = \begin{cases} n^{t=1,2,\dots,N^{itr}} & \text{VESD Type 1} \\ \ln(n^{t=1,2,\dots,N^{itr}}) & \text{VESD Type 2} \end{cases} \tag{14}$$

In (12), *Cov* is the *covariance*,  $\sigma$  is the standard deviation, and  $\rho_{\lambda,\varphi}$  is a *Indicator of Monotonicity* (defined by the Pearson Correlation Coefficient). The closer  $\rho_{\lambda,\varphi}$  is to  $-1$ , the stronger is the monotonic (decreasing) relationship between the model error measure and sample density. If the threshold condition value of  $\rho_{\lambda,\varphi}$  is given by  $\rho_{cr}$ , then  $p = \frac{\rho_{cr}}{\sqrt{(1-\rho_{cr}^2)/d_F}}$  follows a  $t$ -distribution with the degrees

of freedom given by  $d_F = N^{itr} - 2$ . The threshold condition value,  $\rho_{cr}$ , for a  $C_{cr}$  level of confidence can then be determined by

$$\rho_{cr} = \frac{p_{C_{cr},d_F}}{\sqrt{(p_{C_{cr},d_F}^2 + d_F)}} \tag{15}$$

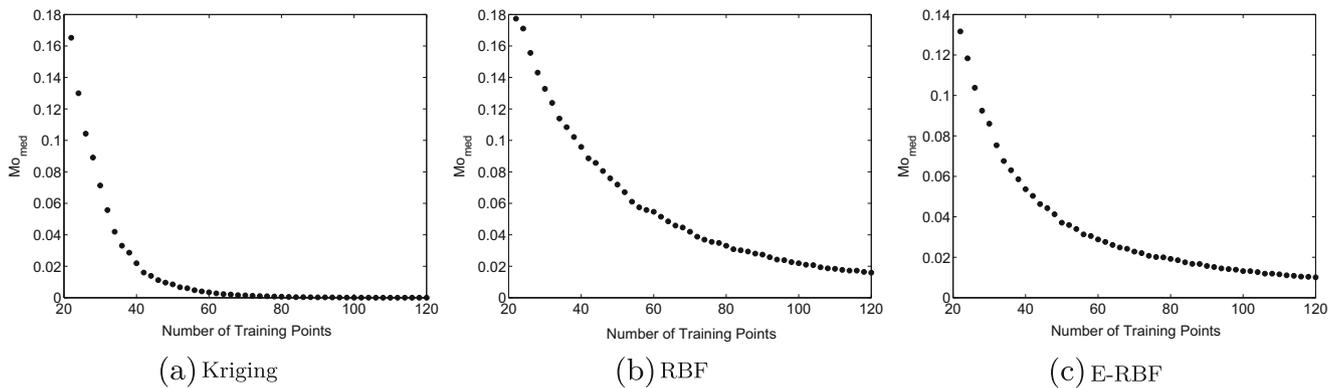
For a given level of confidence ( $C_{cr}$ ), if the *Indicator of Monotonicity*,  $\rho_{\lambda,\varphi}$ , is not greater than the threshold condition value of  $\rho_{cr}$ , the monotonically decreasing characteristics is considered to hold. In that case, the fitted regression function (VESD) is used to predict the fidelity of the final surrogate model ( $VESD(\{X_{in}\})$ ). Conversely, if the *Indicator of Monotonicity* ( $\rho_{\lambda,\varphi}$ ) is greater than the threshold condition value of  $\rho_{cr}$ , the VESD function is discarded, and instead a stable implementation of  $k$ -fold cross-validation (PEMF-based  $k$ -fold) is used, as shown below:

$$E^{PEMF} = \begin{cases} VESD(\{X_{in}\}) & \rho_{\lambda,\varphi} \leq \rho_{cr} \\ Mo^{N^{itr}} & \rho_{\lambda,\varphi} > \rho_{cr} \end{cases} \tag{16}$$

### 2.3 Investigating the stability of PEMF error measures

The individual steps of the PEMF method at each iteration is somewhat analogous to  $k$ -fold cross-validation. In  $k$ -fold cross-validation, errors are generally evaluated for a specific value of  $k$ . In the PEMF method, the errors are evaluated iteratively for different values of  $k$ , in order to predict the level of error in the final surrogate. This novel approach gives PEMF the predictive capability that is otherwise lacking in standard  $k$ -fold or leave-one-out cross-validation. More importantly, PEMF seeks to formulate and use more stable measures of error compared to those in cross-validation. In  $k$ -fold cross-validation, for one specific  $k$ , mean errors are used to represent the level of error, as shown in the pseudo code under Algorithm 1 (in the Appendix). In the PEMF method, the median error on each heuristic set of intermediate test points is first estimated, followed by the determination of the statistical mode of the median errors. The modal error value is then used to represent the level of error at any given  $k$ . The novel use of the modal value of median errors (and similarly modal value of maximum errors) promotes a monotonic decrease of the error measure with sample density, as opposed to the untraceable noisy variation that is often characteristic of mean or RMS error measures.

To illustrate the potential greater stability of PEMF error measures (with respect to their relation to sample density) compared to conventional measures, a two design variable benchmark problem (Branin-Hoo function (Section 3.2)) is considered. The size of the sample data set,  $N$ , is defined to



**Fig. 2** Variation of estimated modal values of median errors with sample density as given by PEMF (Branin-Hoo Function)

be 500, and the region of interest is set to be the entire design space. The numerical settings of this problem is given by

$$N_i = N, n^t = 20 + 2t, \text{ and } M^t = 200, \\ t = 1, 2, 3, \dots, 50$$

Based on this definition, at the first iteration, the intermediate surrogates are constructed using 22 sample points, and tested over 478 points, i.e.,  $N_{TR}^1 = 22$ , and  $N_{TE}^1 = 478$ , where  $N_{TR}^1$  and  $N_{TE}^1$  represent the number of training points and test points, respectively. At the last iteration,  $N_{TR}^{50} = 120$ , and  $N_{TE}^{50} = 380$ .

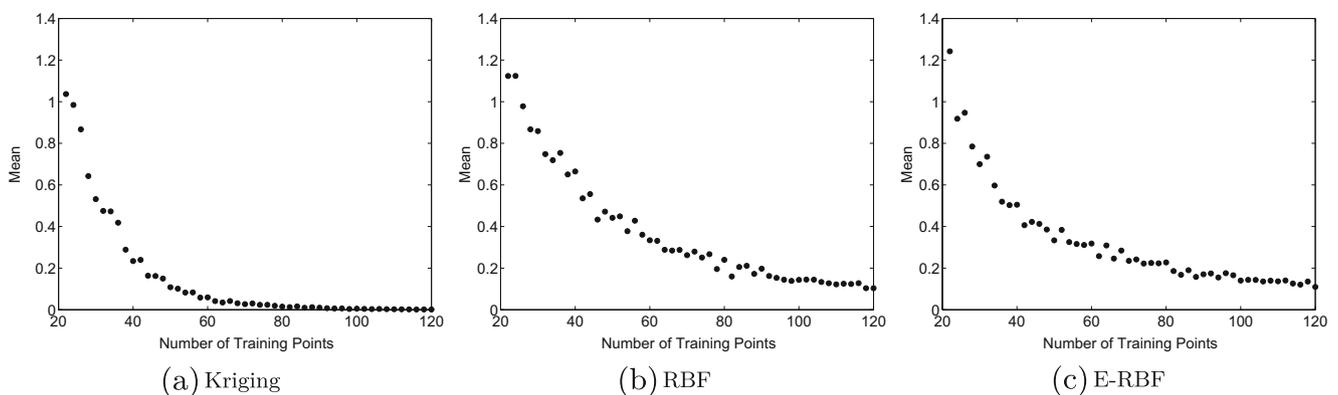
The variation of the *Mode of Median* and the *Mean of the Mean* errors with sample density in different surrogates (Kriging, RBF, and E-RBF) are illustrated in Figs. 2 and 3, respectively. These figures illustrate that the mode of median errors decrease with a practically monotonic trend, with increasing number of training points. Such a monotonic tendency cannot be associated with the *Mean of the Mean* error, as shown in Fig. 3a–c (due to severe local oscillations). It is also important to consider that model errors may not follow a normal distribution, and that the most probable value of error (modal value) might be of greater practical importance (more insightful) than a mean value. From these perspectives, PEMF error measures are likely to

provide a more meaningful understanding of the fidelity of a surrogate model in the context of its use in analysis and design.

### 3 Application of the PEMF method

#### 3.1 Surrogate models

The effectiveness of the PEMF method in predicting the regional and global errors is explored for application with Kriging, RBF, and E-RBF surrogate model on Branin-Hoo function with two design variables, Perm function with 10 design variables, and Dixon & Price function with 50 design variables. The median and the maximum errors evaluated using PEMF are compared with the actual error evaluated on additional test points. To perform a fair comparison, the estimated median and maximum errors on heuristic subsets of additional test points are used to fit error distributions. The statistical mode of the median and the maximum error distributions (estimated over additional test points) are used as reference values (as shown in Algorithm 2 in the Appendix), to investigate performance of PEMF.



**Fig. 3** Variation of typical mean error with sample density, as given by standard  $k$ -fold cross-validation (Branin-Hoo Function)

To illustrate the potential greater effectiveness of the PEMF error metric over popular *cross-validation* error, the mean and maximum errors given by *leave-one-out cross-validation* are also compared with the actual mean and maximum errors. In this case, the mean and the maximum errors estimated on additional test points (as described in Algorithm 3 in the Appendix) are used as reference values.

To implement the Kriging method, the DACE (design and analysis of computer experiments) package developed by Lophaven et al. (2002) is used. The bounds on the correlation parameters in the nonlinear optimization in Kriging,  $\theta_l$  and  $\theta_u$ , are specified to be 0.1 and 20, respectively. In the Kriging surrogate model, the zero-order polynomial function is used as the regression model. To implement the RBF surrogate model, the multiquadric radial basis function (Hardy 1971) is used, where the shape parameter is set to  $c = 0.9$ . In implementing the E-RBF surrogate model (Mullur and Messac 2005), the shape parameter is set to  $c = 0.9$ , the  $\lambda$  parameter is set to 4.75, and the order of monomial in the non-radial basis functions is fixed at 2.

### 3.2 Numerical experiments

PEMF is first applied to the following popular 2D benchmark function:

Branin-Hoo function

$$f(x) = \left( x_2 - \frac{5.1x_1^2}{4\pi^2} + \frac{5x_1}{\pi} - 6 \right)^2 \tag{17}$$

$$+ 10 \left( 1 - \frac{1}{8\pi} \right) \cos(x_1) + 10$$

where  $x_1 \in [-5 \ 10]$ ,  $x_2 \in [0 \ 15]$

The effectiveness of the PEMF method in predicting the global error in high dimensional problems is then explored by applying it to two other analytical benchmark test problems:

– Perm Function (10 variables)

$$f(x) = \sum_{k=1}^n \left\{ \sum_{j=1}^k (j^k + 0.5) \left[ \left( \frac{x_j}{j} \right)^k - 1 \right] \right\}^2 \tag{18}$$

where  $x_i \in [-n \ n + 1]$ ,  $i = 1, \dots, n$

$n = 10$

– Dixon & Price Function (50 variables)

$$f(x) = (x_1 - 1)^2 + \sum_{i=2}^n i (2x_i^2 - x_{i-1})^2 \tag{19}$$

where  $x_i \in [-10 \ 10]$ ,  $i = 1, \dots, n$

$n = 50$

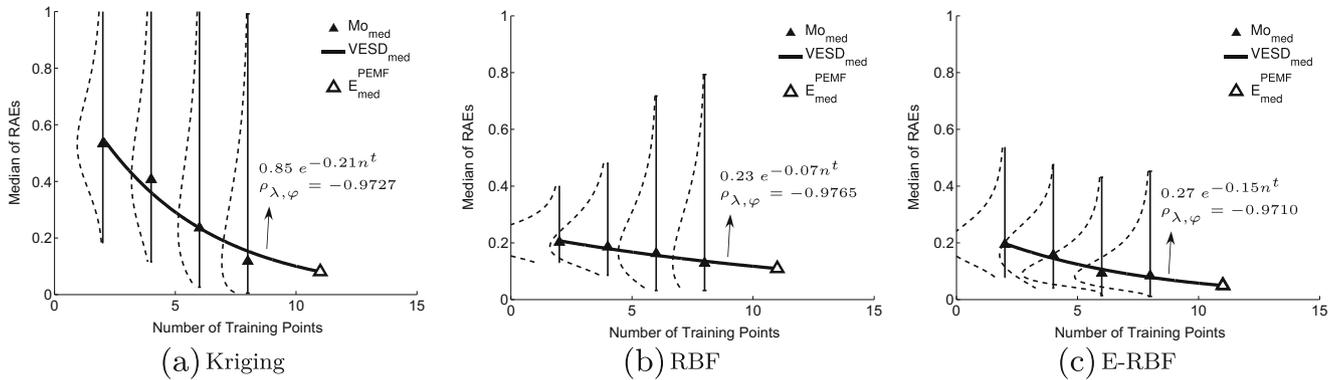
The numerical settings for the application of PEMF in predicting the median and the maximum errors of surrogate models for the benchmark functions are provided in Table 2, which lists (i) the number of training points, (ii) the number of iterations, (iii) the number of inside-region training points based on the predefined region’s boundary, and (iv) the size of the training set at each iteration. Two different cases of error quantification are explored for the Branin-Hoo function. In case I, the PEMF method is used for regional error measurement, where the boundaries of the region of interest are defined as:  $x_1 \in [-2 \ 7]$ ,  $x_2 \in [3 \ 12]$ . While in case II, PEMF is used as a global error measurement method to estimate the model fidelity in entire design domain. To implement the MT criterion, the *threshold condition value* ( $\rho_{cr}$ ) in benchmark problems is estimated to be  $\rho_{cr} = \frac{p_{0.95,2}}{\sqrt{(p_{0.95,2}^2 + 2)}} = -0.950$ , for a specified level of confidence of  $C_{cr} = 0.95$  and  $N^{itr} = 4$ .

### 3.3 Performance criteria

The errors evaluated on additional test points, summarized under Algorithm 2 and Algorithm 3 (in the Appendix), are used to compare the performance of PEMF and *leave-one-out cross-validation*. In this paper, we compare the PEMF method with the popular leave-one-out cross-validation method, particularly with respect to their abilities to predict the quality or fidelity of surrogate models. This comparison is driven by the premise that although these methods are characteristically different the primary ‘end-use’ applications of PEMF and cross-validation methods are similar, namely model testing, model selection, and model

**Table 2** Numerical setup for the benchmark functions

Function	Type of Error Measure	Total No. of sample points, $\{X\}$	No. of iterations, $N^{itr}$	No. of inside-region points, $\{X_{in}\}$	No. of training points at each iteration, $n^t$
Branin-Hoo (Case I)	Regional Error	30	4	11	$2t$
Branin-Hoo (Case II)	Global Error	30	4	30	$19+2t$
Perm	Global Error	50	4	50	$30+4t$
Dixon & Price	Global Error	200	4	200	$150+10t$



**Fig. 4** VESD function to predict the regional median error ( $E_{med}^{PEMF}$ ) in the Branin-Hoo Function (case I)

refinement. The relative differences between the actual errors and the PEMF errors are evaluated as

$$R_{PEMF}^{med} = \left| \frac{E_{Mo-med}^{Actual} - E_{med}^{PEMF}}{E_{Mo-med}^{Actual}} \right| \times 100 \% \tag{20}$$

$$R_{PEMF}^{max} = \left| \frac{E_{Mo-max}^{Actual} - E_{max}^{PEMF}}{E_{Mo-max}^{Actual}} \right| \times 100 \%$$

The relative difference between the actual errors and the errors given by *leave-one-out cross-validation* are evaluated as

$$R_{CV}^{mean} = \left| \frac{E_{mean}^{Actual} - E_{mean}^{CV}}{E_{mean}^{Actual}} \right| \times 100 \% \tag{21}$$

$$R_{CV}^{max} = \left| \frac{E_{max}^{Actual} - E_{max}^{CV}}{E_{max}^{Actual}} \right| \times 100 \%$$

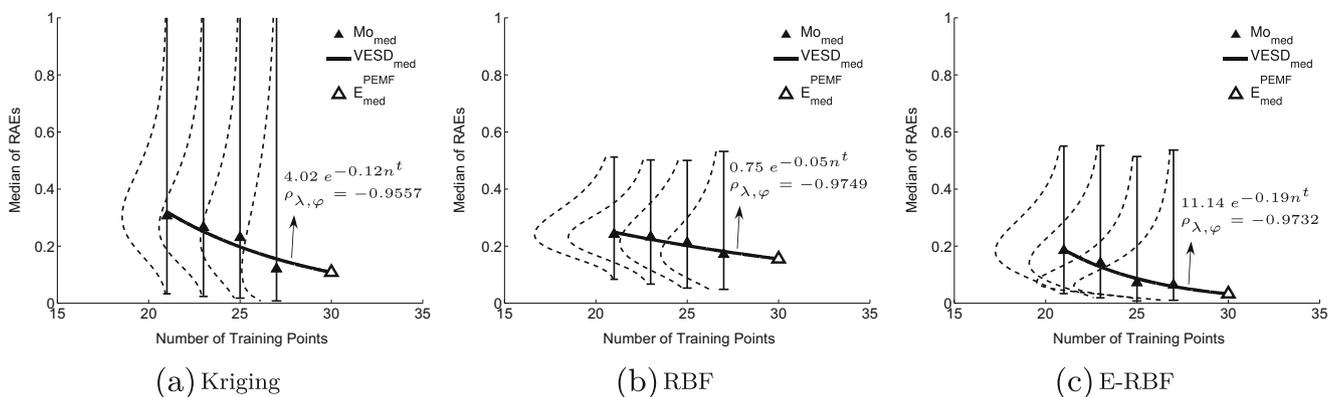
In this study, the number of additional test points used to compare the error measures is equal to 50 times of the number of inside-region samplepoints ( $50 \times N_i$ ).

## 4 Results and discussion

### 4.1 Investigating the performance of PEMF (for the Branin-Hoo function)

Figures 4 and 5 show the VESD regression functions constructed to predict the median errors in the surrogates for Cases I and II, respectively. For the sake of illustration, all the regression coefficients in the figures are rounded to two decimal places. The *Indicator of Monotonicity*,  $\rho_{\lambda, \varphi}$ , for each model is also shown in these figures. The distributions of median errors, and the mode of the median error distributions ( $Mo_{med}$ ) are shown for each iteration. In these figures, the shaded  $\Delta$  symbol represents the quantified mode of median errors at each iteration; the hollow  $\Delta$  symbol represents the predicted mode of median error in the final surrogate.

It is observed from Figs. 4 and 5 that the mode of the error distributions generally decreases with the density of inside-region training points, since the estimated *Indicator of Monotonicity* in the two cases are less

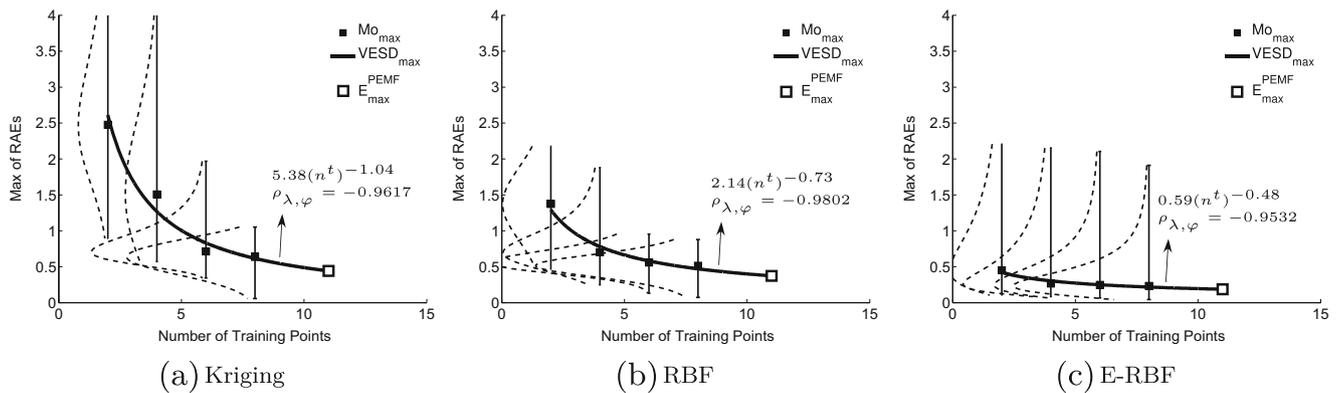


**Fig. 5** VESD function to predict the global median error ( $E_{med}^{PEMF}$ ) in the Branin-Hoo Function (case II)

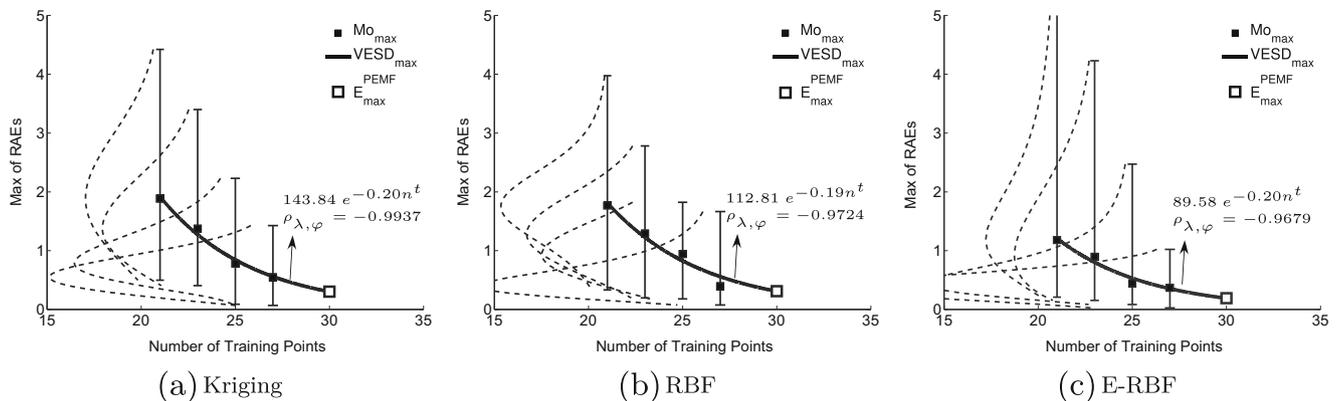
**Table 3** Median error estimated using  $PEMF$  and that estimated on a large pool of additional test points ( $E_{Mo-med}^{Actual}$ )

	Kriging		RBF		E-RBF	
	PEMF	Actual	PEMF	Actual	PEMF	Actual
Regional Modal Error (case I)	0.081	0.088	0.109	0.104	0.049	0.053
Global Modal Error (case II)	0.108	0.097	0.155	0.099	0.033	0.068

Actual: Error evaluated on a large pool of additional test points



**Fig. 6** VESD function to predict the regional maximum error ( $E_{max}^{PEMF}$ ) in the Branin-Hoo Function (case I)

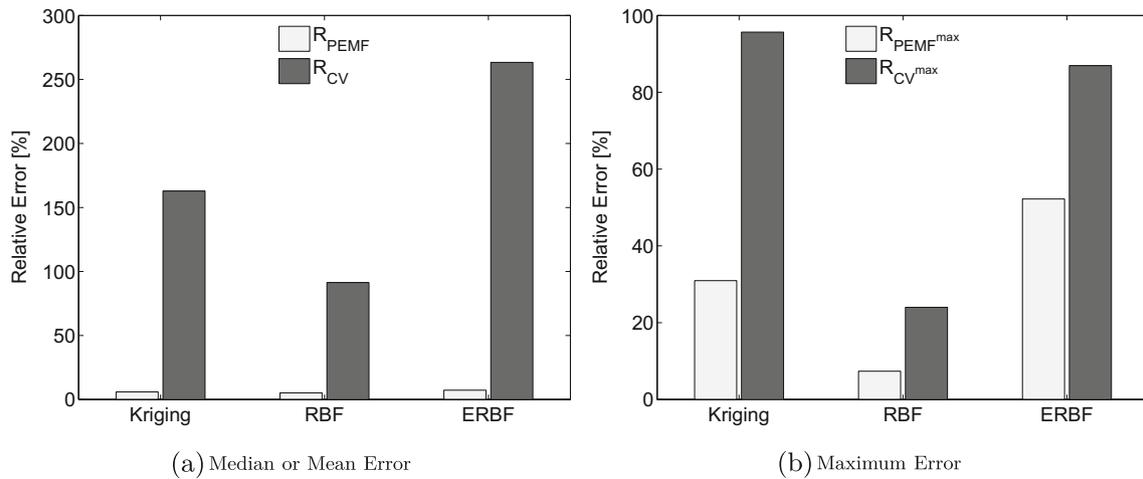


**Fig. 7** VESD function to predict the global maximum error ( $E_{max}^{PEMF}$ ) in the Branin-Hoo Function (case II)

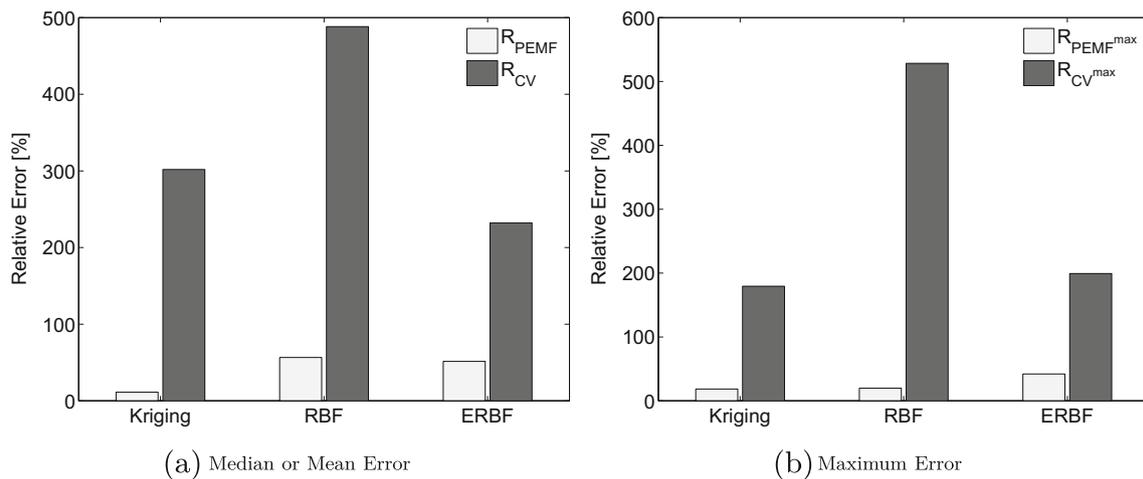
**Table 4** Maximum Error Estimated using  $PEMF$  and that estimated on a large pool of additional test points ( $E_{Mo-max}^{Actual}$ )

	Kriging		RBF		E-RBF	
	PEMF	Actual	PEMF	Actual	PEMF	Actual
Regional Modal Error (case I)	0.442	0.336	0.373	0.402	0.187	0.394
Global Modal Error (case II)	0.358	0.302	0.370	0.309	0.191	0.330

Actual: Error evaluated on a large pool of additional test points



**Fig. 8** Comparison of the *PEFM* and *CV* error measures with the Actual regional error in Branin-Hoo Function (case *I*)



**Fig. 9** Comparison of the *PEFM* and *CV* error measures with the Actual global error in Branin-Hoo Function (case *II*)

**Table 5** Relative differences of the regional errors evaluated using *PEFM* and *CV* from the actual errors in Branin-Hoo Function (case *I*)

	Kriging		RBF		E-RBF	
	$R_{PEFM}^{med}$	$R_{CV}^{mean}$	$R_{PEFM}^{med}$	$R_{CV}^{mean}$	$R_{PEFM}^{med}$	$R_{CV}^{mean}$
Median or Mean Error	<b>7.61 %</b>	162.87 %	<b>4.70 %</b>	91.33 %	<b>6.15 %</b>	263.36 %
Maximum Error	<b>31.18 %</b>	95.66 %	<b>7.07 %</b>	23.99 %	<b>52.63 %</b>	86.92 %

**Table 6** Relative differences of the global errors evaluated using *PEFM* and *CV* from the actual errors in Branin-Hoo Function (case *II*)

	Kriging		RBF		E-RBF	
	$R_{PEFM}^{max}$	$R_{CV}^{max}$	$R_{PEFM}^{max}$	$R_{CV}^{max}$	$R_{PEFM}^{max}$	$R_{CV}^{max}$
Median or Mean Error	<b>11.34 %</b>	301.89 %	<b>56.57 %</b>	488.25 %	<b>51.47 %</b>	232.15 %
Maximum Error	<b>18.54 %</b>	179.49 %	<b>19.74 %</b>	528.38 %	<b>42.12 %</b>	199.36 %

than the pre-estimated threshold ( $\rho_{cr}$ ). Based on these observations, the variation of error with training point density can be represented by applying the VESD regression functions described in Section 2.1.1. The predicted median ( $E_{med}^{PEMF}$ ) errors and actual errors in the final surrogates in Cases *I* and *II* are provided in Table 3. The PEMF error is within the same order of magnitude as the actual errors, which is a significant achievement in surrogate error quantification. It is also important to note that PEMF provides additional helpful insights into the performance of the surrogates for the concerned problem. For example, in these case studies, it is observed (from Figs. 4 and 6) that the regional accuracy of the Kriging surrogate is significantly more sensitive to the sample density than that of the RBF and E-RBF surrogates.

For the two cases of the Branin-Hoo problem, the VESD functions used to predict the mode of the maximum error, and the *Indicator of Monotonicity* ( $\rho_{\lambda, \varphi}$ ) are illustrated in Figs. 6 and 7. The mode of the maximum error distributions in the intermediate surrogate models is represented by the solid square symbol; the hollow square symbol represents the predicted mode of maximum error in the final surrogate. It is again observed that the mode of the maximum error distributions decreases with increasing density of inside-region training points and the *MT criterion* is satisfied in the two cases. The predicted maximum error ( $E_{max}^{PEMF}$ ) and the actual errors evaluated on additional test points (Algorithm 2 in the Appendix) in the final surrogates for Cases *I* and *II* are given in Table 4.

#### 4.1.1 Comparing PEMF with cross-validation (for the Branin-Hoo function)

Figures 8 and 9 illustrate how the PEMF error measure and the RAE given by *leave-one-out cross-validation* compare with the actual error evaluated on additional test points. In these figures, the y-axis represents the relative difference of the error measures compared with the actual errors. These comparisons are given for all three types of surrogate models constructed, i.e., Kriging, RBF, and E-RBF.

The performance criteria defined in Section 3.3 (i.e., R-values in (20) and (21)) are applied to compare the performance of the PEMF method and the *cross-validation* method with the actual errors in Cases *I* and *II*. The comparison results are also provided in Tables 5 and 6. The smaller R-value obtained in each case is shown in boldface. From Figs. 8 and 9 and Tables 5 and 6, it is observed that the measure of surrogate model fidelity provided by the PEMF method is up to two orders of magnitude more accurate than the RAE estimated by *leave-one-out cross-validation*.

## 4.2 Application of PEMF to higher dimensional benchmark problems

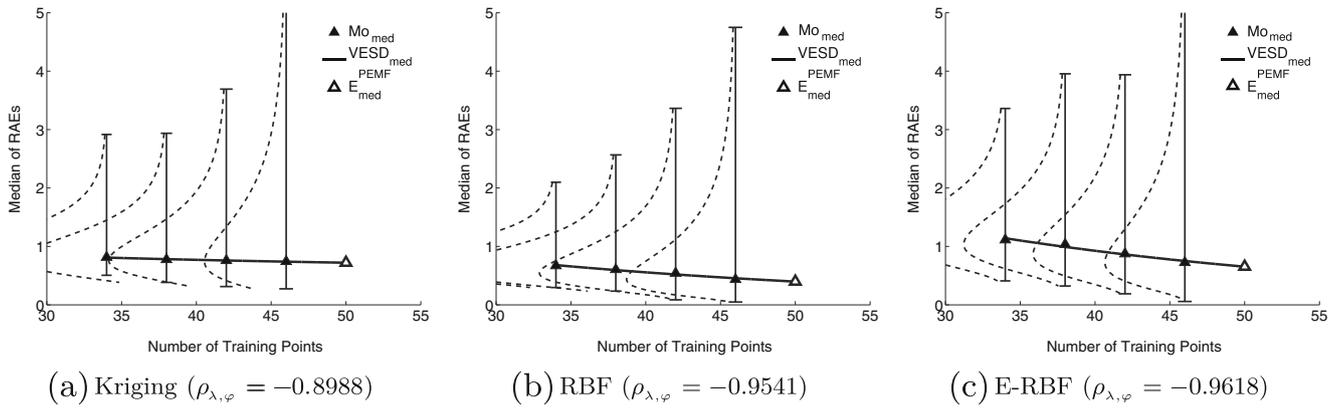
The VESD<sub>med</sub> and VESD<sub>max</sub> regression functions, and the *Indicator of Monotonicity* for the two other benchmark problems, the Perm function (with 10 design variables) and the Dixon & Price function (with 50 design variables), are illustrated in Figs. 10, 11, 12 and 13. It is observed that in most of the cases the *MT criterion* is satisfied, and hence the VESD function can be used to predict the median and maximum errors of the constructed surrogate models. The *MT criterion* is however not satisfied for the following cases: the estimated median error of the Kriging model constructed for the Perm Function (Fig. 10a), and the estimated median error of the RBF model (Fig. 12b) and the estimated maximum error of the Kriging model (Fig. 13a) constructed for the Dixon & Price Function. Therefore, in these three cases, the PEMF-based *k-fold cross-validation* (i.e., the modal value of the error in the last iteration of PEMF) are automatically considered to be the error measure of the surrogate model constructed using all sample points.

The comparison of both the PEMF error measure and the RAE given by *leave-one-out cross-validation* with the actual error evaluated on additional test points are illustrated through bar diagrams in Figs. 14 and 15. In these figures, the y-axis represents the relative difference of the error measures compared with the actual errors. The comparison results are also provided in Tables 7 and 8. A smaller R-value indicates a more accurate error measure. In these tables, the smaller R-values obtained for each case are shown in boldface. From Figs. 14 and 15, and Tables 7 and 8, it is observed that the PEMF method is up to two orders of magnitude more accurate than the *leave-one-out cross-validation* for these 10-50 dimensional test problems. These observations again establish the effectiveness of PEMF as a new more accurate approach to quantify surrogate model errors.

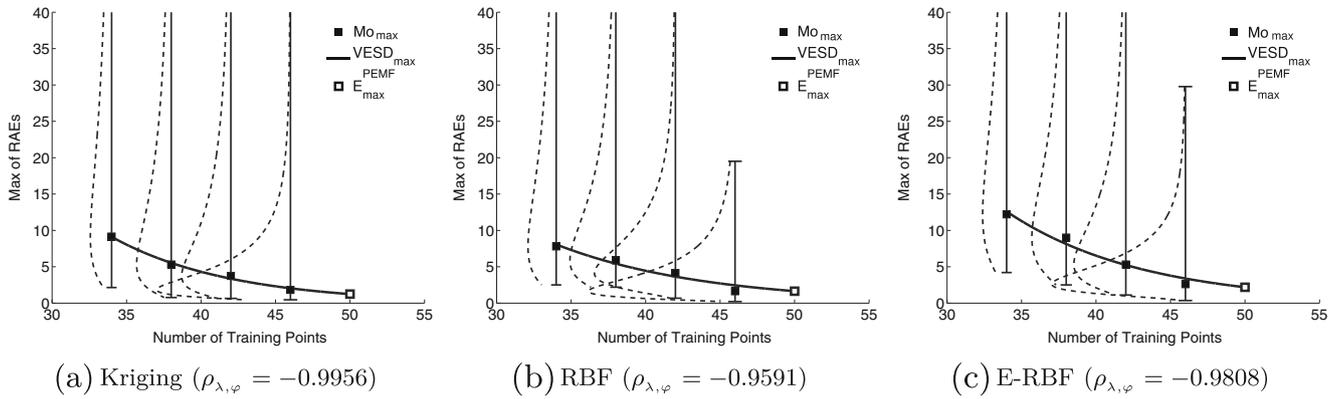
## 5 Statistical test on results of PEMF and leave-one-out cross-validation method

Further statistical tests are performed to illustrate the robustness of the PEMF method. The paired *t*-test (Montgomery and Runger 2010) is applied to measure the significance of the difference between estimated error measures, and the actual error evaluated on additional test points.

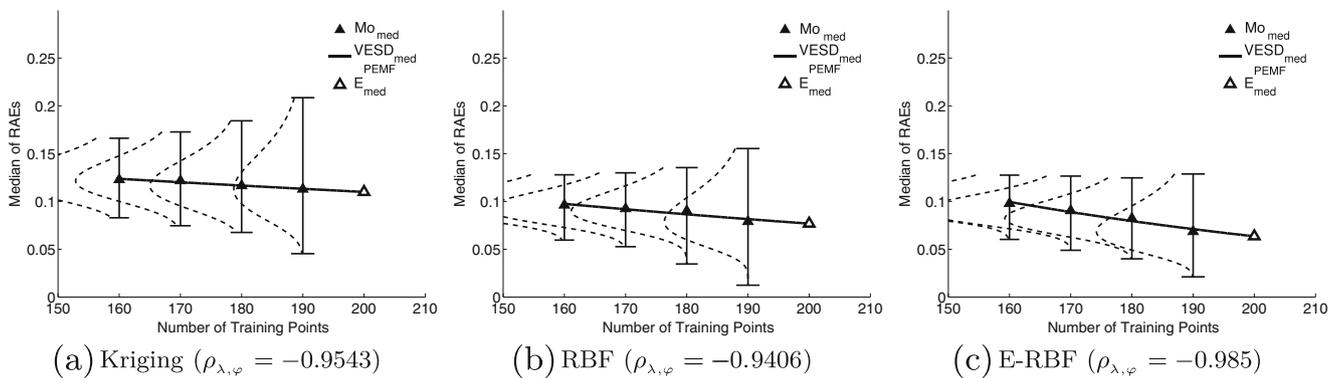
A set of 500 paired sample data is generated using optimal Latin Hypercube, which is defined as  $X_1, X_2, X_3, \dots, X_{500}$ . The size of each sample data set is defined to be  $N_i = 30$ , with all sample points denoted as inside-region sample points, i.e., the PEMF method is applied towards



**Fig. 10** VESD function to predict the global median error ( $E_{med}^{PEMF}$ ) in Perm Function



**Fig. 11** VESD function to predict the global maximum error ( $E_{max}^{PEMF}$ ) in Perm Function



**Fig. 12** VESD function to predict the global median error ( $E_{med}^{PEMF}$ ) in Dixon & Price Function

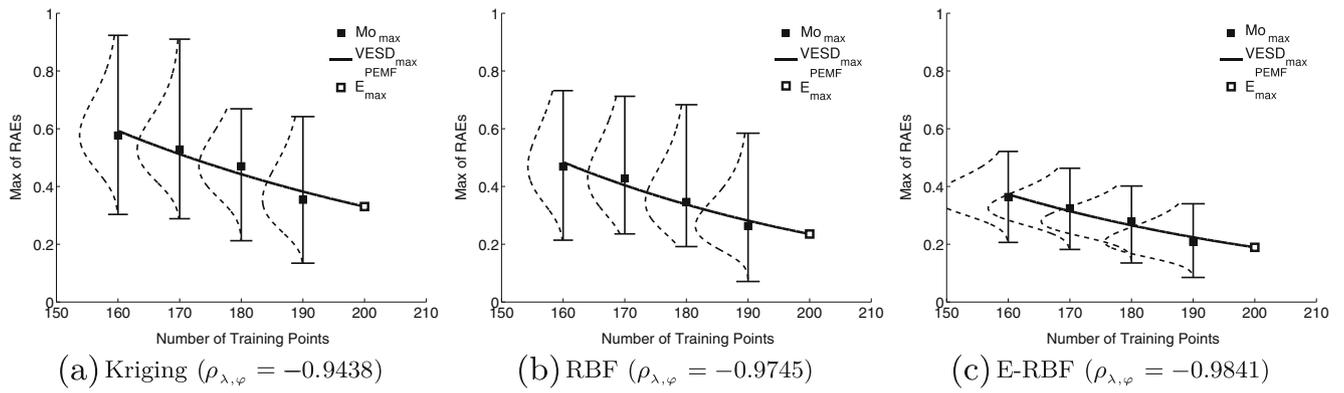


Fig. 13 VESD function to predict the global maximum error ( $E_{max}^{PEMF}$ ) in Dixon & Price Function

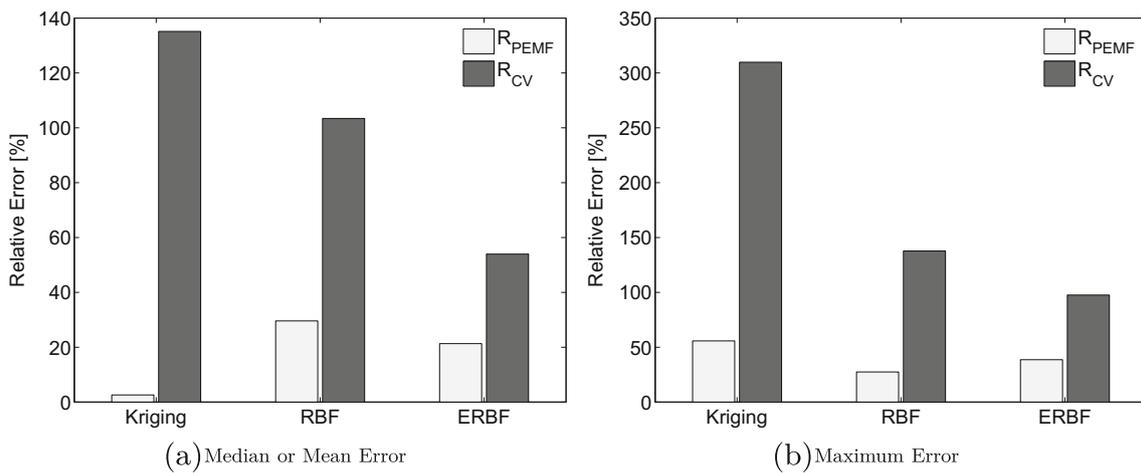


Fig. 14 Comparison of the *PEMF* and *CV* error measures with the Actual global error in Perm Function

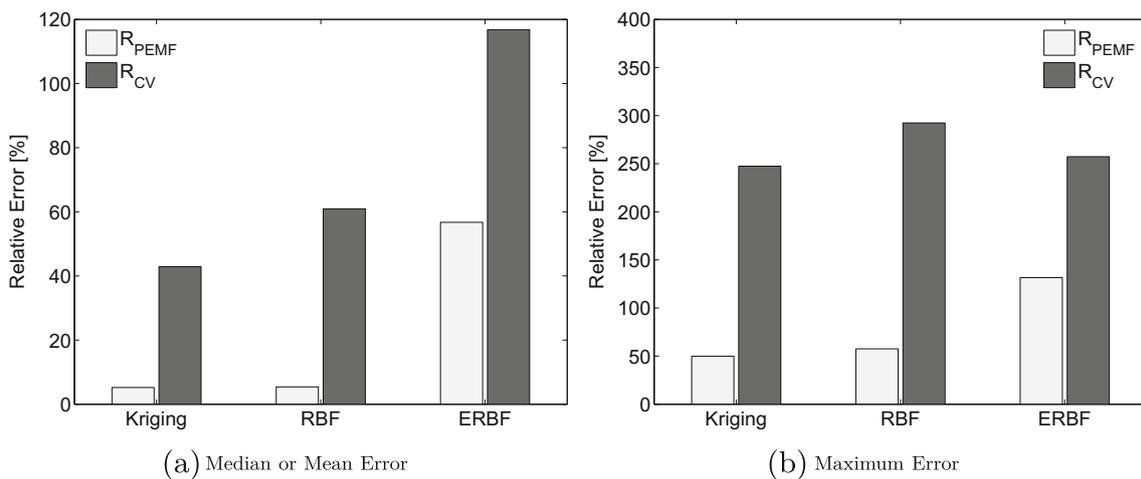


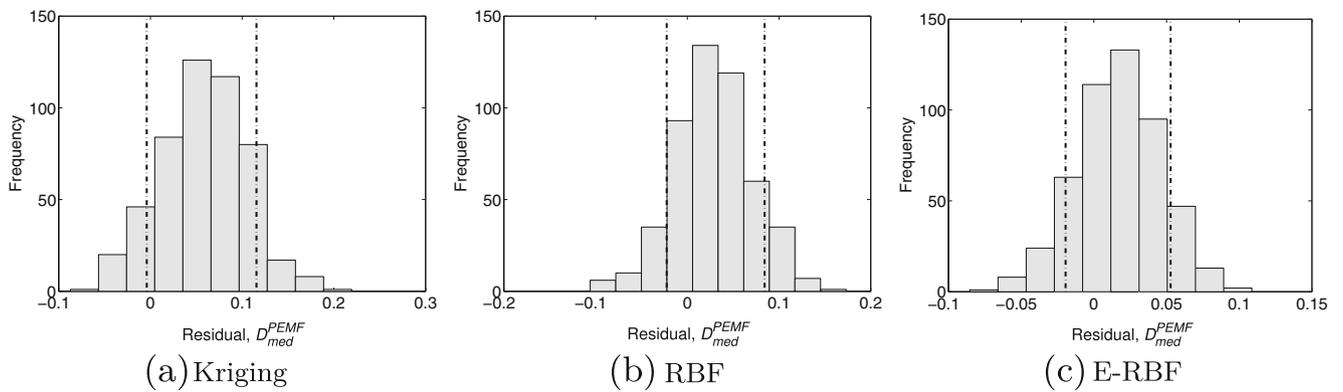
Fig. 15 Comparison of the *PEMF* and *CV* error measures with the Actual global error in Dixon & Price Function

**Table 7** Relative differences of the global errors evaluated using *PEMF* and *CV* from the actual errors in Perm Function

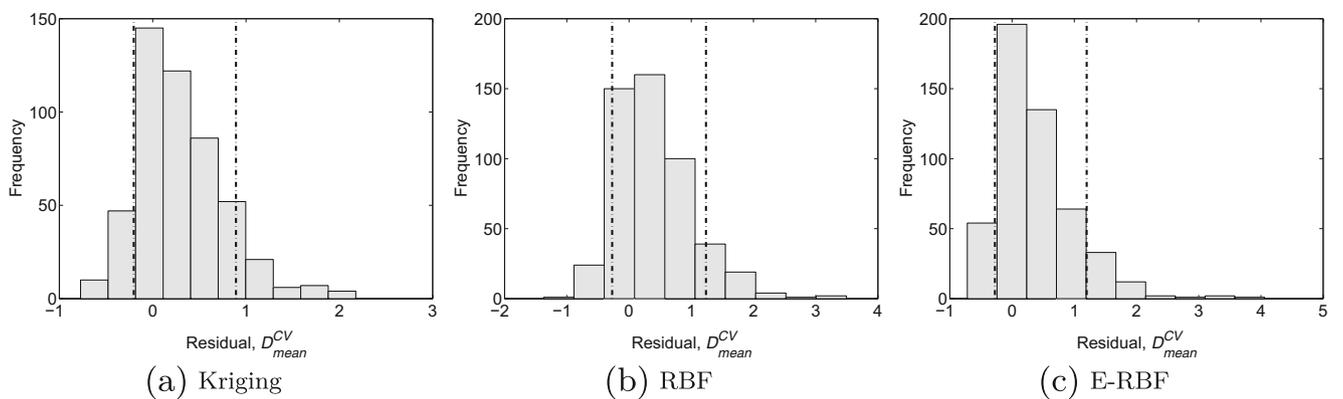
	Kriging		RBF		E-RBF	
	$R_{PEMF}^{med}$	$R_{CV}^{mean}$	$R_{PEMF}^{med}$	$R_{CV}^{mean}$	$R_{PEMF}^{med}$	$R_{CV}^{mean}$
Median or Mean Error	<b>2.61 %</b>	135.11 %	<b>29.60 %</b>	103.40 %	<b>21.32 %</b>	53.96 %
Maximum Error	<b>55.75 %</b>	309.70 %	<b>27.45 %</b>	137.70 %	<b>38.59 %</b>	97.53 %

**Table 8** Relative differences of the global errors evaluated using *PEMF* and *CV* from the actual errors in Dixon & Price Function

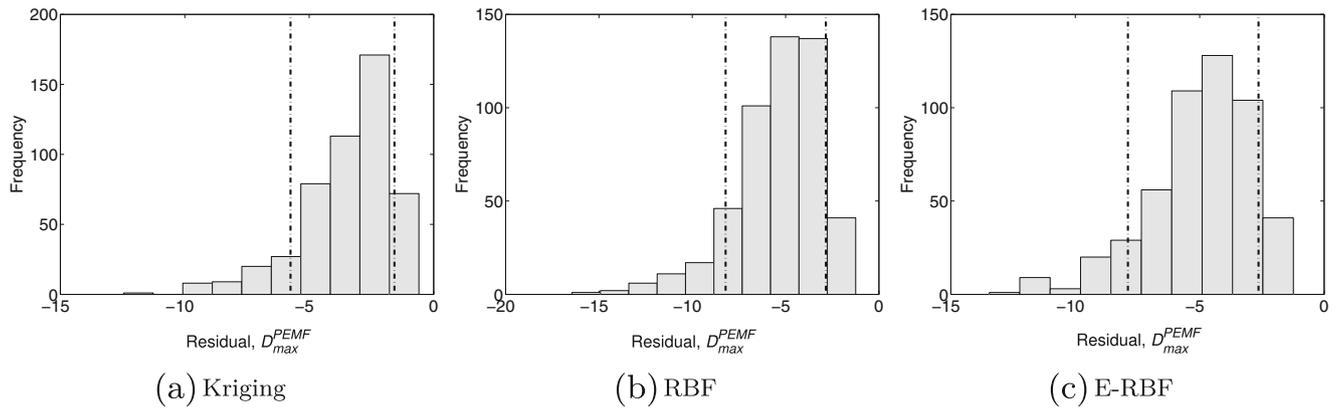
	Kriging		RBF		E-RBF	
	$R_{PEMF}^{max}$	$R_{CV}^{max}$	$R_{PEMF}^{max}$	$R_{CV}^{max}$	$R_{PEMF}^{max}$	$R_{CV}^{max}$
Median or Mean Error	<b>5.20 %</b>	42.88 %	<b>5.39 %</b>	60.93 %	<b>56.72 %</b>	116.79 %
Maximum Error	<b>49.93 %</b>	247.45 %	<b>56.68 %</b>	292.39 %	<b>131.54 %</b>	257.32 %



**Fig. 16** Distribution of the residual of median error estimated using *PEMF* ( $E_{med}^{PEMF}$ ) for Branin-Hoo Function



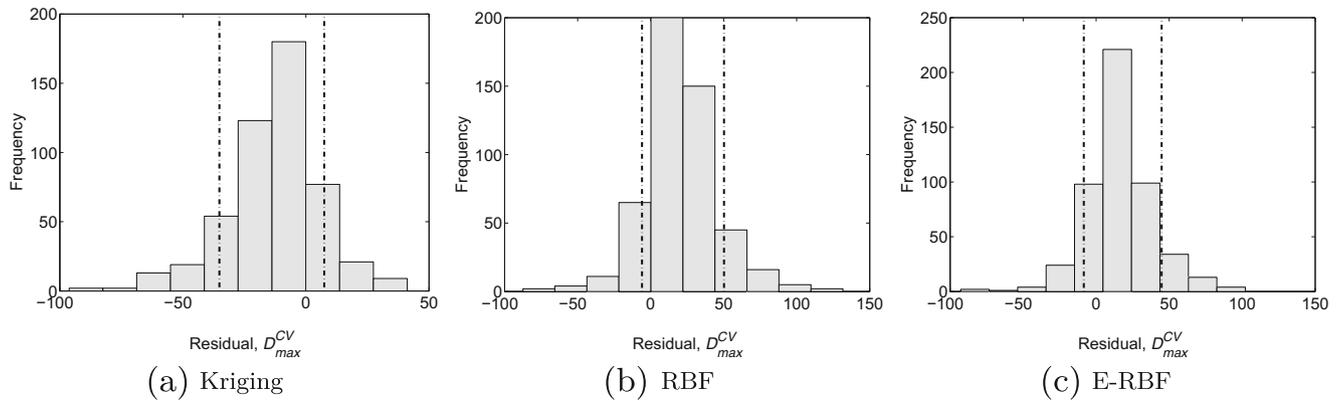
**Fig. 17** Distribution of the residual of mean error estimated using *leave-one-out cross-validation* ( $E_{mean}^{CV}$ ) for Branin-Hoo Function



**Fig. 18** Distribution of the residual of maximum error estimated using PEMF ( $E_{max}^{PEMF}$ ) for Branin-Hoo Function

**Table 9** 90 % bootstrapped confidence intervals for residuals of  $E_{med}^{PEMF}$  (given by PEMF) and  $E_{mean}^{CV}$  (given by CV) in different surrogates

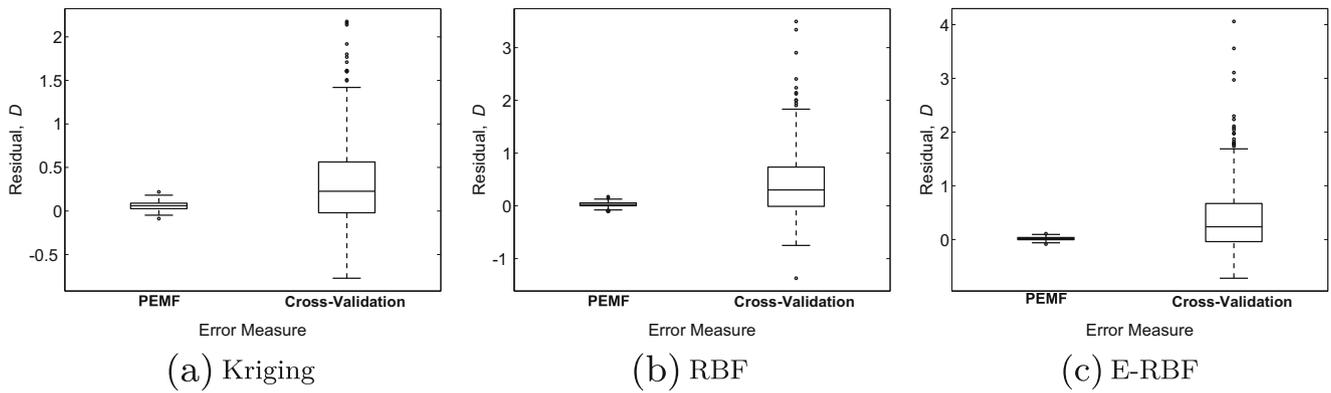
Measure	Kriging	RBF	E-RBF
$E_{med}^{PEMF}$	$0.057 \leq \mu_D \leq 0.059$	$0.028 \leq \mu_D \leq 0.029$	$0.017 \leq \mu_D \leq 0.017$
$E_{mean}^{CV}$	$0.296 \leq \mu_D \leq 0.299$	$0.400 \leq \mu_D \leq 0.404$	$0.373 \leq \mu_D \leq 0.377$



**Fig. 19** Distribution of the Residual of maximum error estimated using *leave-one-out cross-validation*  $E_{max}^{CV}$  for Branin-Hoo Function

**Table 10** 90 % bootstrapped CIs for residuals of  $E_{max}^{PEMF}$  (given by PEMF) and  $E_{max}^{CV}$  (given by CV) in different surrogates

Measure	Kriging	RBF	E-RBF
$E_{max}^{PEMF}$	$-3.479 \leq \mu_D \leq -3.469$	$-5.389 \leq \mu_D \leq -5.376$	$-4.991 \leq \mu_D \leq -4.980$
$E_{max}^{CV}$	$-12.934 \leq \mu_D \leq -12.829$	$20.175 \leq \mu_D \leq 20.317$	$16.344 \leq \mu_D \leq 16.473$



**Fig. 20** Interquartile Range box plot of the residuals of the central tendency of surrogate errors (median in PEMF; and mean in *leave-one-out cross-validation*) for the Branin-Hoo Function

global error measurement. In this test, it is assumed that the size of the inside-region training set at each iteration,  $t$ , is given by

$$n^t = \left\lfloor \frac{N_i}{N^{itr} + 1} t \right\rfloor \tag{22}$$

where the function  $\lfloor x \rfloor$  returns the largest integer less than or equal to  $x$ . The differences between the errors estimated using PEMF and the actual error on each pair of observation are defined as

$$D_{med}^{PEMF} = E_{med}^{PEMF} - E_{Mo-med}^{Actual} \tag{23}$$

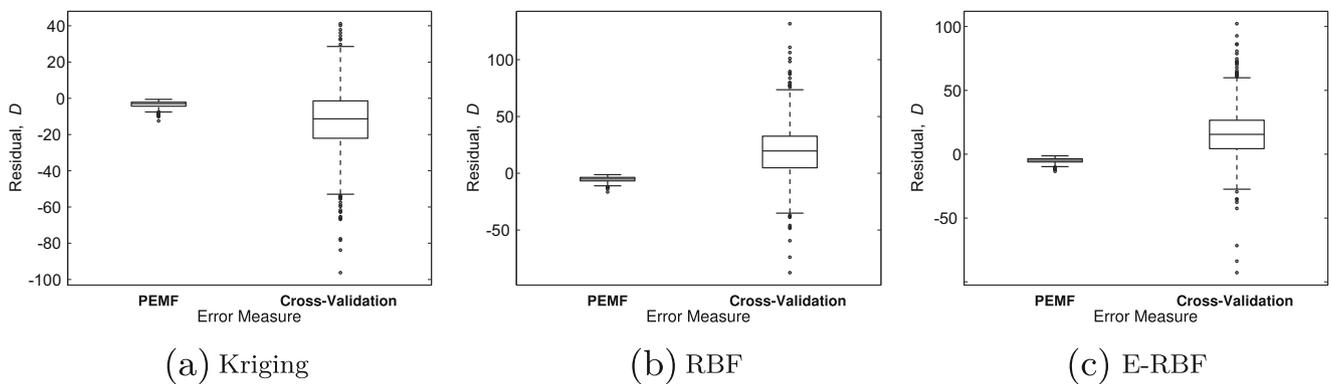
$$D_{max}^{PEMF} = E_{max}^{PEMF} - E_{Mo-max}^{Actual}$$

The frequency histogram of the residuals in different types of surrogates (Kriging, RBF, and E-RBF) for the median and maximum errors estimated using PEMF are illustrated in Figs. 16 and 18, respectively. The frequency histogram of the residuals in different types of surrogates (Kriging, RBF, and E-RBF) for the mean and maximum errors estimated using leave-one-out cross validation are illustrated in Figs. 17 and 19, respectively. In these figures, the 10th and the 90th percentiles of the residuals are illustrated using black dashed lines.

It is readily evident from the histograms in Figs. 16 and 18 that the residuals do not necessarily follow a normal distribution. Hence, statistical methods based on a resampling approach such as the Bootstrapping method should be applied to perform the statistical inference (Efron and Tibshirani 1993). In the Bootstrapping method, it is assumed that the statistics of the sampling distribution is the probability of all possible values of the estimated statistics calculated from a sample of size  $n$  drawn from a given population (Haukoos and Lewis 2005). To evaluate the 90 % bootstrap confidence intervals (CI), after creating  $n$  bootstrapped sets from the original residuals, the mean value for each bootstrapped data set is independently computed. The 90 % CI from the set of computed mean values are then estimated using the normal approximation method. Assuming the normal approximation is normally distributed with sample mean  $\bar{d}^*$  and standard deviation  $s_D^*$  for the  $n = 1000$  bootstrapped resamples, a 90 % confidence interval on the difference in means,  $\mu_D$ , is defined as

$$\bar{d}^* - t_{0.05, n-1} \times \frac{s_D^*}{\sqrt{n}} \leq \mu_D \leq \bar{d}^* + t_{0.05, n-1} \times \frac{s_D^*}{\sqrt{n}} \tag{24}$$

In this case,  $t_{0.05, n-1}$  is the upper 0.05 % point of the  $t$  distribution with  $n - 1$  degrees of freedom. Confidence intervals



**Fig. 21** Interquartile range box plot of the residuals of the maximum surrogate error for the Branin-Hoo Function

that are narrower and closer to zero indicate higher level of robustness of the error measurement.

Table 9 presents the 90 % confidence intervals (CI) for residuals of the mode of median and maximum errors estimated using the PEMF method in different surrogates.

Likewise, the statistical test is also performed for *leave-one-out* cross-validation. In this test, the same 500 paired sample data are used where the differences between the mean and maximum errors estimated by the *cross-validation* method and the actual error on each pair of observation are given by

$$D_{mean}^{CV} = E_{mean}^{CV} - E_{mean}^{Actual} \quad (25)$$

$$D_{max}^{CV} = E_{max}^{CV} - E_{max}^{Actual}$$

The actual errors are errors evaluated on additional test points, as given by Algorithm 3 (in the Appendix).

The frequency histogram of the residuals in different types of surrogates (Kriging, RBF, and E-RBF), for the mean and maximum errors estimated using *cross-validation*, are illustrated in Figs. 17 and 19, respectively. We again use the normal approximation method to estimate the 90 % bootstrapped confidence intervals on the difference in the means,  $\mu_D$ , for the residuals of errors, which are reported in Table 10.

To compare the PEMF method and the *leave-one-out cross-validation* method, the distribution of the residuals of each surrogate is described by a box plot. The box plot indicates the deviation of the central tendency from zero (which is the expected value). Figures 20 and 21 respectively illustrate the distribution of residuals of the median and the maximum errors estimated using PEMF, and the mean error and the maximum errors estimated using *cross-validation* in different surrogates. From the results of the statistical test on PEMF and *cross-validation* (Figs. 16, 17, 18, 19, 20 and 21 and Tables 9 and 10), it is readily evident that the confidence intervals and the 25th and 75th percentiles for PEMF are significantly closer to zero (up to two orders of magnitude closer) compared to that for *cross-validation*. These observations show that PEMF is expected to provide far superior robustness in quantifying surrogate model errors compared to standard *leave-one-out cross-validation*.

## 6 Conclusion

This paper develops a new approach to quantify the accuracy of surrogate models in a given region of the design domain or the entire design domain. Such an approach is useful for informed decision-making when using surrogate models or metamodels for analysis and optimization. This method, called the *Predictive Estimation of Model Fidelity*

(PEMF), is a model-independent method for predicting the error in the actual surrogate model constructed using all available sample points. In this method, intermediate surrogates are constructed iteratively using multiple heuristic subsets of the available sample points. The remaining sample points are used to evaluate the error in the estimated function at that iteration. In this method, the model error at each iteration is defined by the mode of the median error and the maximum error distributions – this is expected to promote greater stability compared to mean or mean squared error measures. Regression models are then developed to represent the error in the surrogate as a function of the density of training points. These regression models are then extrapolated to predict the fidelity of the final surrogate model under the condition that a *Monotonic Trend (MT) criterion* is satisfied. The *MT criterion* is a mechanism to statistically test the feasibility of the monotonic relationship between the modal error values and training sample density. If the *MT criterion* is not satisfied, the estimated modal error values from the last iteration is used to represent the measure of fidelity of the surrogate model – which is essentially a more stable implementation of *k*-fold cross-validation. The effectiveness of the new PEMF method is illustrated by applying it to a 2-variable, a 10-variable, and a 50-variable benchmark problems, where the following types of surrogate models were constructed: Kriging, RBF, and E-RBF surrogates. These numerical experiments show that the PEMF method provides up to two orders of magnitude greater accuracy in measuring surrogate model error compared to the relative absolute error estimated by *leave-one-out cross-validation*. Superior robustness of the PEMF method is also established using additional statistical tests.

At this point, the number of iterations and the initial ratio of the numbers of intermediate training points to test points have to be prescribed by the user. Hence there remains scope for exploring strategies that adaptively determine these two factors as functions of the dimension and strength of the sample data, thereby making PEMF more tractable. The application of PEMF to a wide variety of complex engineering design problems, particularly in the context of model refinement, model selection, and uncertainty analysis will further establish the diverse potential of this novel approach to quantify the fidelity of surrogate models.

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## Appendix A

### A.1 Standard $k$ -fold cross-validation

---

#### Algorithm 1

---

**INPUT:**

 Set  $k$ 

 Set  $N = \binom{N_i}{k}$ 

```

for  $j = 1, 2, \dots, N$  do
  for  $i = 1, 2, \dots, K$  do
    Estimate actual value on  $i^{th}$  training point;  $y_i = \text{System}(x_i)$ 
    Estimate predicted value on  $i^{th}$  training point;  $\hat{y}_i = \text{Surrogate}(x_i)$ 
    Estimate RAE on  $i^{th}$  training point;  $RAE_i = \left| \frac{y_i - \hat{y}_i}{y_i} \right|$ 
  end for
  Evaluate mean of the relative absolute errors value;
   $E_j = \text{mean}(RAE_i), i = 1, 2, \dots, K$ 
end for
  Evaluate mean of the mean errors value;
   $E^{k\text{-fold}} = \text{mean}(E_j), j = 1, 2, \dots, N$ 

```

---

### A.2 Quantifying the mode of median and maximum errors, estimated on additional test points (for performance testing of PEMF)

---

#### Algorithm 2

---

**INPUT:**

 Set Number of additional test points  $N^{test}$ 

 Set Size of combinations,  $n$  ( $n < N^{test}$ )

 Set Number of combinations,  $P$  ( $P < \binom{N^{test}}{n}$ )

```

for  $i = 1, 2, \dots, N^{test}$  do
  Estimate actual value on  $i^{th}$  test point;  $y_i = \text{System}(x_i)$ 
  Estimate predicted value on  $i^{th}$  test point;  $\hat{y}_i = \text{Surrogate}(x_i)$ 
  Estimate RAE on  $i^{th}$  test point;  $RAE_i = \left| \frac{y_i - \hat{y}_i}{y_i} \right|$ 
end for
for  $j = 1, 2, \dots, P$  do
  Select a random subset of size  $n$  from RAEs,
  Evaluate the median and maximum of the selected RAEs value  $RAE_{med}$  and  $RAE_{max}$ ;
   $RAE_{med} = \text{median}(RAE_i), RAE_{max} = \max(RAE_i)$ ,
  and  $i = 1, 2, \dots, n$ .
end for
  Fit a distribution of the median and the maximum errors over all  $P$  combinations

  Determine the mode of the error distributions;  $E_{Mo-med}^{Actual}$  and  $E_{Mo-max}^{Actual}$ 

```

---

### A.3 Quantifying the mean and the maximum errors estimated on additional test points (for performance testing of cross-validation)

---

#### Algorithm 3

---

**INPUT:**

 Set Number of additional test points,  $N^{test}$ 

```

for  $i = 1, \dots, N^{test}$  do
  Estimate actual value on  $i^{th}$  test point;  $y_i = \text{System}(x_i)$ 
  Estimate predicted value on  $i^{th}$  test point;  $\hat{y}_i = \text{Surrogate}(x_i)$ 
  Estimate RAE on  $i^{th}$  test point;  $RAE_i = \left| \frac{y_i - \hat{y}_i}{y_i} \right|$ 
end for
  Evaluate the mean and maximum of the relative absolute errors value;
   $E_{mean}^{Actual} = \text{mean}(RAE_i)$  and  $E_{max}^{Actual} = \max(RAE_i)$ ,
   $i = 1, 2, \dots, N^{test}$ 

```

---

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