

1. PROBLEMA DIRECTO (Obtención coordenadas UTM)

a) Obtención de la longitud de arco de meridiano.

$$l.a.m. = s_m = m \cdot \varphi - n \cdot \text{sen}2\varphi + p \cdot \text{sen}4\varphi - q \cdot \text{sen}6\varphi$$

$$A = 1 + \frac{3}{4} \cdot e^2 + \frac{45}{64} \cdot e^4 + \frac{175}{256} \cdot e^6$$

$$B = \frac{3}{4} \cdot e^2 + \frac{15}{16} \cdot e^4 + \frac{525}{512} \cdot e^6$$

$$C = \frac{15}{64} \cdot e^4 + \frac{105}{256} \cdot e^6$$

$$D = \frac{35}{512} \cdot e^6$$

$$m = A \cdot a \cdot (1 - e^2) \quad n = \frac{B}{2} \cdot a \cdot (1 - e^2)$$

$$p = \frac{C}{4} \cdot a \cdot (1 - e^2) \quad q = \frac{D}{6} \cdot a \cdot (1 - e^2)$$

b) Determinación de K_0 , N y η

$$\varphi < 36^\circ \rightarrow K_0 = 0,999333333$$

$$\varphi > 40^\circ \rightarrow K_0 = 0,9996$$

$$\eta'^2 = e'^2 \cdot \cos^2 \varphi'$$

c) Obtención de las coordenadas ϕ y λ .

$$x = 500.000 + K_0 \cdot (\lambda \cdot N \cdot \cos \varphi + \frac{\lambda^3}{6} \cdot N \cdot \cos^3 \varphi \cdot (1 - \text{tg}^2 \varphi + \eta^2) + \frac{\lambda^5}{120} \cdot N \cdot \cos^5 \varphi \cdot (5 - 18 \text{tg}^2 \varphi + \text{tg}^4 \varphi + 14 \eta^2 - 58 \eta^2 \cdot \text{tg}^2 \varphi + 13 \eta^4 - 64 \eta^4 \cdot \text{tg}^2 \varphi + 4 \eta^6 - 24 \eta^6 \cdot \text{tg}^2 \varphi))$$

$$y = K_0 \cdot (s_m + \frac{\lambda^2}{2} \cdot N \cdot \text{tg} \varphi \cdot \cos^2 \varphi + \frac{\lambda^4}{24} \cdot N \cdot \text{tg} \varphi \cdot \cos^4 \varphi \cdot (5 - \text{tg}^2 \varphi + 9 \eta^2 + 4 \eta^4) + \frac{\lambda^6}{720} \cdot N \cdot \text{tg} \varphi \cdot \cos^6 \varphi \cdot (61 - 58 \text{tg}^2 \varphi + \text{tg}^4 \varphi + 270 \eta^2 - 330 \eta^2 \cdot \text{tg}^2 \varphi + 445 \eta^4 - 680 \eta^4 \cdot \text{tg}^2 \varphi + 324 \eta^6 - 600 \eta^6 \cdot \text{tg}^2 \varphi + 88 \eta^8 - 192 \eta^8 \cdot \text{tg}^2 \varphi))$$

2. PROBLEMA INVERSO (Obtención coordenadas geodésicas).

a) Obtención de x e y

$$x = \frac{x - 500.000}{K_0}$$

$$y = \frac{N}{K_0}$$

b) Obtención de ϕ en función de la $s_m' = y$.

$$l.a.m.(\varphi') = s_m' = a \cdot (1 - e^2) \cdot (g_1 + g_2 + g_3 + g_4 + g_5 + g_6)$$

$$\varphi'_1 = \frac{s_m'}{a \cdot (1 - e^2)}$$

$$g_1 = \varphi'$$

$$g_2 = \frac{3}{2} \cdot e'^2 \cdot (-\frac{1}{2} \cdot \text{sen} \varphi' \cdot \text{cos} \varphi' + \frac{1}{2} \varphi')$$

$$g_3 = \frac{15}{8} \cdot e'^4 \cdot (-\frac{1}{4} \cdot \text{sen}^3 \varphi' \cdot \text{cos} \varphi' - \frac{3}{8} \cdot \text{sen} \varphi' \cdot \text{cos} \varphi' + \frac{3}{8} \varphi')$$

$$g_4 = \frac{35}{16} \cdot e'^6 \cdot (-\frac{1}{6} \cdot \text{sen}^5 \varphi' \cdot \text{cos} \varphi' - \frac{5}{24} \cdot \text{sen}^3 \varphi' \cdot \text{cos} \varphi' - \frac{5}{16} \cdot \text{sen} \varphi' \cdot \text{cos} \varphi' + \frac{5}{16} \varphi')$$

$$g_5 = \frac{315}{128} \cdot e'^8 \cdot (-\frac{1}{8} \cdot \text{sen}^7 \varphi' \cdot \text{cos} \varphi' - \frac{7}{48} \cdot \text{sen}^5 \varphi' \cdot \text{cos} \varphi' - \frac{35}{192} \cdot \text{sen}^3 \varphi' \cdot \text{cos} \varphi' - \frac{35}{128} \cdot \text{sen} \varphi' \cdot \text{cos} \varphi' + \frac{35}{128} \varphi')$$

$$g_6 = \frac{693}{256} \cdot e'^{10} \cdot (-\frac{1}{10} \cdot \text{sen}^9 \varphi' \cdot \text{cos} \varphi' - \frac{9}{80} \cdot \text{sen}^7 \varphi' \cdot \text{cos} \varphi' - \frac{21}{160} \cdot \text{sen}^5 \varphi' \cdot \text{cos} \varphi' - \frac{21}{128} \cdot \text{sen}^3 \varphi' \cdot \text{cos} \varphi' - \frac{63}{256} \cdot \text{sen} \varphi' \cdot \text{cos} \varphi' + \frac{63}{256} \varphi')$$

c) Cálculo de la longitud y la latitud.

$$\lambda = \frac{x}{N' \cdot \cos \varphi'} - \frac{x^3}{6 \cdot N'^3 \cdot \cos^3 \varphi'} \cdot (1 + 2 \text{tg}^2 \varphi' + \eta'^2) + \frac{x^5}{120 \cdot N'^5 \cdot \cos^5 \varphi'} \cdot (5 + 28 \text{tg}^2 \varphi' + 24 \text{tg}^4 \varphi' + 6 \eta'^2 + 8 \eta'^2 \cdot \text{tg}^2 \varphi' - 3 \eta'^4 \cdot \text{tg}^2 \varphi' - 4 \eta'^6 + 24 \eta'^6 \cdot \text{tg}^2 \varphi')$$

$$\varphi = \varphi' - \frac{x^2}{2 \cdot N'^2} \cdot \text{tg} \varphi' \cdot (1 + \eta'^2) + \frac{x^4}{24 \cdot N'^4} \cdot \text{tg} \varphi' \cdot (5 + 3 \text{tg}^2 \varphi' + 6 \eta'^2 - 6 \eta'^2 \cdot \text{tg}^2 \varphi' - 3 \eta'^4 - 9 \eta'^4 \cdot \text{tg}^2 \varphi') - \frac{x^6}{720 \cdot N'^6} \cdot \text{tg} \varphi' \cdot (61 + 90 \text{tg}^2 \varphi' + 45 \text{tg}^4 \varphi' + 107 \eta'^2 - 162 \eta'^2 \cdot \text{tg}^2 \varphi' - 45 \eta'^2 \cdot \text{tg}^4 \varphi' + 43 \eta'^4 - 318 \eta'^4 \cdot \text{tg}^2 \varphi' + 135 \eta'^4 \cdot \text{tg}^4 \varphi' + 97 \eta'^6 + 18 \eta'^6 \cdot \text{tg}^2 \varphi' + 225 \eta'^6 \cdot \text{tg}^4 \varphi' + 188 \eta'^8 - 108 \eta'^8 \cdot \text{tg}^2 \varphi' + 88 \eta'^{10} - 192 \eta'^{10} \cdot \text{tg}^2 \varphi')$$

CONVERGENCIA DE MERIDIANOS.

a) A partir de coordenadas UTM.

$$\gamma = \frac{x}{N'} \cdot \operatorname{tg} \varphi' - \frac{x^3}{3 \cdot N'^3} \cdot \operatorname{tg} \varphi' \cdot (1 + \operatorname{tg}^2 \varphi' - \eta'^2 - 2\eta'^4) + \frac{x^5}{15 \cdot N'^5} \cdot \operatorname{tg} \varphi' \cdot (2 + 5\operatorname{tg}^2 \varphi' + 3\operatorname{tg}^4 \varphi')$$

b) A partir de las coordenadas geodésicas.

$$\gamma = \lambda \cdot \operatorname{sen} \varphi + \frac{\lambda^3}{3} \cdot \operatorname{sen} \varphi \cdot \cos^2 \varphi \cdot (1 + 3\eta^2 + 2\eta^4) + \frac{\lambda^5}{15} \cdot \operatorname{sen} \varphi \cdot \cos^4 \varphi \cdot (2 - \operatorname{tg}^2 \varphi)$$

3. CÁLCULO DEL MÓDULO DE DEFORMACIÓN LINEAL PUNTUAL.

a) En coordenadas geodésicas.

$$K_1 = K_o \cdot \left(1 + \frac{1}{2} \cdot \lambda^2 \cdot \cos^2 \varphi \cdot (1 + \eta^2) + \frac{1}{24} \cdot \lambda^4 \cdot \cos^4 \varphi \cdot (5 - 4\operatorname{tg}^2 \varphi + 14\eta^2 - 28\eta^2 \cdot \operatorname{tg}^2 \varphi + 13\eta^4 - 48\eta^4 \cdot \operatorname{tg}^2 \varphi + 4\eta^6 - 24\eta^6 \cdot \operatorname{tg}^2 \varphi) \right)$$

b) En coordenadas UTM.

$$K_1 = K_o \cdot \left(1 + \frac{x^2}{2 \cdot \rho' \cdot N'} + \frac{x^4}{24 \cdot N'^4} \cdot (1 + 6\eta'^2 + 9\eta'^4 - 24 \cdot \operatorname{tg}^2 \varphi' \cdot \eta'^4 + 4\eta'^6 - 24\operatorname{tg}^2 \varphi' \cdot \eta'^6) \right)$$

c) Expresión simplificada.

Coord. Geodésicas	Coord. UTM
$K_1 = K_o \cdot \left(1 + \frac{1}{2} \cdot \lambda^2 \cdot \cos^2 \varphi \cdot (1 + \eta^2) \right)$	$K_1 = K_o \cdot \left(1 + \frac{x^2}{2 \cdot N'^2} \cdot (1 + \eta'^2) \right)$

4. DISTINTOS PARÁMETROS A OBTENER.

- Distancia UTM.

$$D_{UTM} = \sqrt{\Delta x^2 + \Delta y^2}$$

- Distancia sobre el elipsoide (Arco).

$$D_2 = \frac{D_{UTM}}{K_1}$$

- Distancia sobre el elipsoide (Cuerda).

$$D_2 = D_1 + \frac{D_1^3}{24 \cdot R^2}$$

- Distancia reducida a un horizonte medio

$$K_h = R = 1 - \frac{H_m}{R_T} + \frac{H_m^2}{R_T^2} = \frac{D_1}{D_R}$$

- Distancia sobre la cuerda a partir de Dg

$$D_1 = \left(\frac{D_g^2 - \Delta H^2}{\left(1 + \frac{H_A}{R} \right) \cdot \left(1 + \frac{H_B}{R} \right)} \right)^{1/2}$$

- Acimut cartográfico.

$$(\theta)_{c.c.} = \operatorname{arctg} \left(\frac{\Delta x}{\Delta y} \right)$$

- Reducción angular de la cuerda.

$$dT_{B1}^P = \frac{(y_P - y_{B1}) \cdot (2x_{B1} + x_P)}{6 \cdot N_m \cdot \rho_m} \cdot (1 + \eta_m^2)$$

- Acimut geodésico de la geodesia.

$$(\theta_{B1}^P)_g = ((\theta_{B1}^P)_{c.c.} + dT_{B1}^P) + \gamma_{B1}$$

- Coordenadas de B respecto de A.

$$\begin{aligned} X_B &= X_A + (D_A^B)_{UTM} \cdot \text{sen}(\theta_A^B)_{\text{cuerda}} \\ Y_B &= Y_A + (D_A^B)_{UTM} \cdot \text{cos}(\theta_A^B)_{\text{cuerda}} \end{aligned}$$

- Cálculo de K1 para distancias

$$K_1 = K_0 \cdot \left(1 + \frac{1}{2 \cdot N^2} \cdot (1 + \eta'^2) \cdot \frac{1}{K_0^2} \cdot 10^{12} \cdot q_m^2 \right)$$

$$\text{siendo: } q_m = \frac{q_A + q_B}{2}$$

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